# STRUCTURAL CALCULATIONS 

Steinborn Residence

8435 SE $47^{\text {th }}$ PL,
Mercer Island, WA 98040

Ectypos Architecture
4212 W Mercer Way,
Mercer Island, WA 98040
February 14, 2022
Structural Permit
Calculations




All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $863 @ 41 / 2^{\prime \prime}$ | $1679(3.50 ")$ | Passed (51\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $821 @ 51 / 2^{\prime \prime}$ | 1903 | Passed (43\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Member Type : Joist |  |  |  |  |  |
| Building Use : Residential |  |  |  |  |  |
| Moment (Ft-lbs) | $3816 @ 9 ' 7 "$ | 4364 | Passed (87\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Live Load Defl. (in) | $0.539 @ 9^{\prime} 7 "$ | 0.921 | Passed (L/410) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $0.808 @ 99^{\prime \prime}$ | 1.228 | Passed (L/273) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 288 | 575 | 863 | Blocking |
| 2-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 283 | 565 | 848 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime} 8{ }^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | 19 o o/c |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.
-Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $19^{\prime}$ | $24 "$ | 15.0 | 30.0 | Roof Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
| Bykonen Carter Quinn |  |
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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $1088 @ 23^{\prime} 71 / 2^{\prime \prime}$ | $1731(3.50 ")$ | Passed (63\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $1046 @ 31 / 2^{\prime \prime}$ | 1961 | Passed (53\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Member Type : Joist |  |  |  |  |  |
| Building Use : Residential |  |  |  |  |  |
| Building Code : IBC 2018 |  |  |  |  |  |
| Moment (Ft-lbs) | $6169 @ 11^{\prime} 11^{\prime \prime}$ | 7107 | Passed (87\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Live Load Defl. (in) | $1.043 @ 11^{\prime} 11^{\prime \prime}$ | 1.171 | Passed (L/270) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $1.564 @ 11^{\prime} 11^{\prime \prime}$ | 1.561 | Passed (L/180) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 358 | 715 | 1073 | Blocking |
| 2-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 363 | 725 | 1088 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime} 6{ }^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $24^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.
-Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $24^{\prime}$ | $24^{\prime \prime}$ | 15.0 | 30.0 | Roof Load |

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Roof, J3
1 piece(s) $2 \times 4$ HF No. 2 @ 24" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $213 @ 1^{\prime} 101 / 4^{\prime \prime}$ | $2126(3.50 ")$ | Passed (10\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $71 @ 1^{\prime} 5^{\prime \prime}$ | 604 | Passed (12\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Moment (Ft-lbs) | $-59 @ 1^{\prime} 101 / 4^{\prime \prime}$ | 430 | Passed (14\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.008 @ 3^{\prime}$ | 0.200 | Passed (2L/999+) | -- | $1.0 \mathrm{D}+1.0$ S (Alt Spans) |
| Total Load Defl. (in) | $0.011 @ 3^{\prime}$ | 0.200 | Passed (2L/999+) | -- | $1.0 \mathrm{D}+1.0$ S (Alt Spans) |

System : Roof Member Type : Joist Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: $\mathrm{LL}\left(2 \mathrm{~L} / 0.2^{\prime \prime}\right)$ and $\mathrm{TL}\left(2 \mathrm{~L} / 0.2^{\prime \prime}\right)$.
- Right cantilever length exceeds $1 / 3$ member length or $1 / 2$ back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 19 | 50 | 69 | Blocking |
| 2-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50 "$ | 71 | 142 | 213 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime}$ o/c |  |
| Bottom Edge (Lu) | $3^{\prime}$ o/c |  |

$\bullet$ Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $3^{\prime}$ | $24 \prime$ | 15.0 | 30.0 | Roof Load |

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Roof, J4
2 piece(s) $2 \times 4$ HF No. 2 @ 24" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $515 @ 2^{\prime} 73 / 4^{\prime \prime}$ | $4253(3.50 ")$ | Passed (12\%) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Shear (lbs) | $237 @ 3^{\prime} 1^{\prime \prime}$ | 1208 | Passed (20\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | $-315 @ 2^{\prime} 73 / 4^{\prime \prime}$ | 861 | Passed (37\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.111 @ 0$ | 0.265 | Passed (2L/572) | -- | $1.0 \mathrm{D}+1.0$ S (Alt Spans) |
| Total Load Defl. (in) | $0.146 @ 0$ | 0.353 | Passed (2L/434) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (Alt Spans) |

System : Roof Member Type : Joist Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: $\operatorname{LL}(2 \mathrm{~L} / 240)$ and $\mathrm{TL}(2 \mathrm{~L} / 180)$.
- Left cantilever length exceeds $1 / 3$ member length or $1 / 2$ back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 172 | 343 | 515 | Blocking |
| 2-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50 "$ | 53 | 129 | 182 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $7^{\prime} 6 " \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $7^{\prime} 6 \mathrm{o} ~ \mathrm{o} \mathrm{c}$ |  |

$\bullet$-Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location (Side) | Spacing | Dead <br> $(\mathbf{0 . 9 0})$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $7^{\prime} 6 "$ | $24^{\prime \prime}$ | 15.0 | 30.0 | Roof Load |

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1 piece(s) 3 1/2" $\times 11$ 7/8" 1.55E TimberStrand® LSL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $3009 @ 2 "$ | $4961(3.50 ")$ | Passed (61\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $1724 @ 11^{\prime} 33 / 8^{\prime \prime}$ | 9878 | Passed (17\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Moment (Ft-lbs) | $4026 @ 3 '$ | 18346 | Passed (22\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.030 @ 3^{\prime}$ | 0.283 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $0.045 @ 3^{\prime}$ | 0.378 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

System : Roof
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Available | Required | Dead | Snow | Total | Accessories |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.12^{\prime \prime}$ | 1029 | 1980 | 3009 | Blocking |
| 2 - Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.12^{\prime \prime}$ | 1029 | 1980 | 3009 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime}$ o/c |  |
| Bottom Edge (Lu) | 6 ' o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to 6' | $\mathrm{N} / \mathrm{A}$ | 13.0 | -- |  |
| 1 - Uniform (PSF) | 0 to $6^{\prime}$ (Front) | $22^{\prime}$ | 15.0 | 30.0 | Roof Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Roof <br> Member Type : Flush Beam <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD <br> Member Pitch : 0/12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1264 @ 3 1/2" | 4725 (1.50") | Passed (27\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Shear (lbs) | 1162 @ 1' 3 3/8" | 9878 | Passed (12\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |
| Moment (Ft-lbs) | 7754 @ 12' 6 3/4" | 18346 | Passed (42\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Live Load Defl. (in) | 0.663 @ 12' 6 3/4" | 1.227 | Passed (L/444) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Total Load Defl. (in) | 1.138 @ 12' 6 3/4" | 1.636 | Passed (L/259) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Available | Required | Dead | Snow | Total | Accessories |  |
| 1-Hanger on 11 7/8" HF beam | $3.50^{\prime \prime}$ | Hanger $^{1}$ | $1.50^{\prime \prime}$ | 536 | 754 | 1290 | See note ${ }^{1}$ |
| 2 - Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 535 | 746 | 1281 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $24^{\prime} 9{ }^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $24^{\prime} 9{ }^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

## Connector: Simpson Strong-Tie

| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - Face Mount Hanger | LUS410 | $2.00 "$ | N/A | $8-10 \mathrm{dx} 1.5$ | $6-10 \mathrm{~d}$ |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | $31 / 2^{\prime \prime}$ to $25^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.0 | -- |  |
| 1 - Uniform (PSF) | 0 to $25^{\prime}$ (Front) | $2^{\prime}$ | 15.0 | 30.0 |  |

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ForteWEB Software Operator
J ob Notes

Roof, J7
2 piece(s) 1 3/4" x 3 1/ 2" 2.0E Microllam® LVL @ 24" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 818 @ 4' 1 3/4" | 4961 (3.50") | Passed (16\%) | -- | 1.0 D + 1.0 S (All Spans) |
| Shear (lbs) | 406 @ 4'7" | 2677 | Passed (15\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | -773@ 4' 1 3/4" | 2190 | Passed (35\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Live Load Defl. (in) | 0.374 @ 0 | 0.415 | Passed (2L/266) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (Alt Spans) |
| Total Load Defl. (in) | 0.481 @ 0 | 0.553 | Passed (2L/206) | -- | 1.0 D + 1.0 S (Alt Spans) |

System : Roof Member Type : Joist Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: $\operatorname{LL}(2 \mathrm{~L} / 240)$ and $\mathrm{TL}(2 \mathrm{~L} / 180)$.
- Left cantilever length exceeds $1 / 3$ member length or $1 / 2$ back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A $4 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Resawn products must maintain manufacturing stamps.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | 3.50" | 3.50 " | 1.50 " | 273 | 546 | 819 | Blocking |
| 2 - Stud wall - HF | 3.50" | 3.50 " | 1.50" | 87 | 208 | 295 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} \mathrm{o} / \mathrm{c}$ |  |

$\bullet$ Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $12^{\prime}$ | $24 \prime \prime$ | 15.0 | 30.0 | Roof Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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| Bykonen Carter Quinn |  |
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| jaj@bcq-se.com |  |

1 piece(s) 3 1/ 2" x 11 7/ 8" 1.55E TimberStrand® LSL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Roof <br> Member Type : Flush Beam <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD <br> Member Pitch : 0/12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 978 @ 2" | 4961 (3.50") | Passed (20\%) | -- | 1.0 D + 1.0 S (All Spans) |  |
| Shear (lbs) | 846 @ 1' 3 3/8" | 9878 | Passed (9\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |
| Moment (Ft-lbs) | 4486 @ 9' 6" | 18346 | Passed (24\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |
| Live Load Defl. (in) | 0.226 @ 9' 6" | 0.933 | Passed (L/992) | -- | 1.0 D + 1.0 S (All Spans) |  |
| Total Load Defl. (in) | 0.388 @ 9' 6" | 1.244 | Passed (L/578) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | 3.50" | 3.50 " | 1.50 " | 408 | 570 | 978 | Blocking |
| 2 - Stud wall - HF | 3.50" | 3.50 " | 1.50" | 408 | 570 | 978 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | 19 o o/c |  |
| Bottom Edge (Lu) | $19 \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to $199^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.0 | -- |  |
| 1 - Uniform (PSF) | 0 to $19^{\prime}$ (Front) | $2^{\prime}$ | 15.0 | 30.0 |  |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Roof <br> Member Type : Flush Beam <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD <br> Member Pitch : 0/12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 3799 @ 4' 4" | 4961 (3.50") | Passed (77\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Shear (lbs) | 2514 @ 3' 2 5/8" | 9878 | Passed (25\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |
| Moment (Ft-lbs) | 3951 @ 2' 11 11/16" | 18346 | Passed (22\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |
| Live Load Defl. (in) | 0.018 @ 2' 3 7/16" | 0.208 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Total Load Defl. (in) | 0.029 @ 2' 3 7/16" | 0.278 | Passed (L/999+) | -- | 1.0 D + 1.0 S (All Spans) |  |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.10^{\prime \prime}$ | 1074 | 1909 | 2983 | Blocking |
| 2-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.68 "$ | 1414 | 2385 | 3799 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} 6 "$ o/c |  |
| Bottom Edge (Lu) | $4^{\prime} 6^{\prime \prime}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> (0.90) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0-Self Weight (PLF) | 0 to 4' 6' | N/A | 13.0 | -- |  |
| 1- Uniform (PSF) | 0 to 4' 6" (Front) | $22^{\prime}$ | 15.0 | 30.0 | Roof Load |
| 2- Point (lb) | $3^{\prime}$ (Front) | N/A | 536 | 754 | Linked from: B6, <br> Support 1 |
| 3- Point (lb) | 3' (Front) | N/A | 408 | Linked from: B8, <br> Support 2 |  |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $5028 @ 11 / 2^{\prime \prime}$ | $9844(3.00 ")$ | Passed (51\%) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Shear (lbs) | $4204 @ 1^{\prime} 21 / 4^{\prime \prime}$ | 13132 | Passed (32\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Member Type : Header |  |  |  |  |  |
| Moment (Ft-lbs) | $17602 @ 7^{\prime} 3^{\prime \prime}$ | 30998 | Passed (57\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Live Load Defl. (in) | $0.357 @ 7^{\prime} 3 \prime$ | 0.475 | Passed (L/478) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $0.551 @ 7^{\prime} 3^{\prime \prime}$ | 0.712 | Passed (L/310) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1- Trimmer - DF | $3.00 "$ | $3.00^{\prime \prime}$ | $1.53 "$ | 1765 | 3263 | 5028 | None |
| 2 - Trimmer - DF | $3.00 "$ | $3.00^{\prime \prime}$ | $1.53 "$ | 1765 | 3263 | 5028 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :---: | :---: | :---: |
| Top Edge (Lu) | 14'6" o/c |  |
| Bottom Edge (Lu) | 14' 6" o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $14^{\prime} 6^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 18.5 | -- |  |
| 1 - Uniform (PSF) | 0 to $14^{\prime} 6^{\prime \prime}$ | $15^{\prime}$ | 15.0 | 30.0 | Snow |

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## Roof, Roof header, $8^{\prime}$ opening

## 3 piece(s) $\mathbf{2} \mathbf{x} \mathbf{1 0}$ HF No. 2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Wall <br> Member Type : Header <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology: ASD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 2914 @ 1 1/2" | 5468 (3.00") | Passed (53\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Shear (lbs) | 2214 @ 1' 1/4" | 4787 | Passed (46\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Moment (Ft-lbs) | 5832 @ 4' 3" | 5750 | Passed (101\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Live Load Defl. (in) | 0.122 @ 4' 3" | 0.275 | Passed (L/814) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Total Load Defl. (in) | 0.185 @ 4' 3" | 0.412 | Passed (L/535) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1- Trimmer - DF | $3.00 "$ | $3.00^{\prime \prime}$ | $1.60^{\prime \prime}$ | 1001 | 1913 | 2914 | None |
| 2 - Trimmer - DF | $3.00 "$ | $3.00^{\prime \prime}$ | $1.60^{\prime \prime}$ | 1001 | 1913 | 2914 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $8^{\prime} 6 \mathrm{o} ~ \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $(\mathbf{0 . 9 0})$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $8^{\prime} 6^{\prime \prime}$ | N/A | 10.6 | -- |  |
| 1 - Uniform (PSF) | 0 to $8^{\prime} 6^{\prime \prime}$ | $15^{\prime}$ | 15.0 | 30.0 | Snow |

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## Roof, Roof header, 6' opening

## 2 piece(s) $\mathbf{2 \times 8} \mathbf{~ H F}$ No. 2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Wall <br> Member Type : Header <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology: ASD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1700 @ 11/2" | 3645 (3.00") | Passed (47\%) | -- | 1.0 D + 1.0 S (All Spans) |  |  |
| Shear (lbs) | 1253 @ $101 / 4{ }^{\prime \prime}$ | 2501 | Passed (50\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |  |
| Moment (Ft-lbs) | 2554 @ 3' ${ }^{\prime \prime}$ | 2569 | Passed (99\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Live Load Defl. (in) | 0.096 @ 3' 3' | 0.208 | Passed (L/784) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Total Load Defl. (in) | 0.145 @ 3' 3" | 0.313 | Passed (L/517) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1- Trimmer - DF | $3.00^{\prime \prime}$ | $3.00^{\prime \prime}$ | $1.50^{\prime \prime}$ | 579 | 1121 | 1700 | None |
| 2 - Trimmer - DF | $3.00^{\prime \prime}$ | $3.00^{\prime \prime}$ | $1.50^{\prime \prime}$ | 579 | 1121 | 1700 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $1^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $6^{\prime} 6 \mathrm{o}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $6^{\prime} 6^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 5.5 | -- |  |
| 1 - Uniform (PSF) | 0 to $6^{\prime} 6^{\prime \prime}$ | $11^{\prime} 6 \prime$ | 15.0 | 30.0 | Snow |

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Roof, Trellis joist, see Risa for steel framing
1 piece(s) $2 \times 4$ HF No. 2 @ 24" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $545 @ 44^{\prime} 51 / 4^{\prime \prime}$ | $2126(3.50 ")$ | Passed (26\%) | -- | $1.0 \mathrm{D}+1.0$ S (Adj Spans) |
| Shear (lbs) | $250 @ 4^{\prime} 101 / 2^{\prime \prime}$ | 604 | Passed (41\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (Adj Spans) |
| Member Type : Joist |  |  |  |  |  |
| Moment (Ft-lbs) | $-276 @ 4^{\prime} 51 / 4^{\prime \prime}$ | 430 | Passed (64\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (Adj Spans) |
| Live Load Defl. (in) | $0.110 @ 7^{\prime} 7 \prime$ | 0.315 | Passed (L/684) | -- | $1.0 \mathrm{D}+1.0$ S (Alt Spans) |
| Total Load Defl. (in) | $0.153 @ 7^{\prime} 7^{\prime \prime}$ | 0.419 | Passed (L/494) | -- | $1.0 \mathrm{D}+1.0$ S (Alt Spans) |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Beam - DF | 3.50" | 3.50 " | 1.50" | 49 | 113 | 162 | Blocking |
| 2 - Beam - DF | 3.50" | 3.50 " | 1.50" | 179 | 366 | 545 | None |
| 3-Beam - DF | 3.50 " | 3.50 " | 1.50" | 179 | 366 | 545 | None |
| 4 - Beam - DF | 3.50" | 3.50 " | 1.50" | 49 | 113 | 162 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $15^{\prime} 2^{\prime \prime} 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $13^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $15^{\prime} 2^{\prime \prime}$ | $24^{\prime \prime}$ | 15.0 | 30.0 | Default Load |

## Weyerhaeuser Notes

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www.weyerhaeuser.com/woodproducts/document-library.
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
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| (206) 264-7784 |  |
| jaj@bcq-se.com |  |



|  | Label | $\mathrm{X}[\mathrm{ft}]$ | Y [ft] | Z [ft] | Temp [deg F] | Detach From Diap... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N3 | 0 | 6.5 | 2.3 |  |  |
| 2 | N4 | 14.4 | 6.5 | 2.3 |  |  |
| 3 | N5 | 0 | 7.5 | 12.2 |  |  |
| 4 | N6 | 14.4 | 7.5 | 12.2 |  |  |
| 5 | N9 | 14.4 | 0 | 12.2 |  |  |
| 6 | N10 | 0 | 0 | 12.2 |  |  |
| 7 | N11 | 14.4 | 7.732323 | 14.5 |  |  |
| 8 | N12 | 0 | 7.732323 | 14.5 |  |  |
| 9 | N9A | 4 | 6.5 | 2.3 |  |  |
| 10 | N10A | 4 | 7.732323 | 14.5 |  |  |
| 11 | N11A | 10.4 | 6.5 | 2.3 |  |  |
| 12 | N12A | 10.4 | 7.732323 | 14.5 |  |  |
| 13 | N13 | 4 | 7.5 | 12.2 |  |  |
| 14 | N14 | 10.4 | 7.5 | 12.2 |  |  |

## Boundary Conditions

| Node Label |  | X [k/in] | Y [k/in] | Z [k/in] | X Rot [k-ft/rad] | Y Rot [k-ft/rad] | Z Rot [k-ft/rad] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N3 | Reaction | Reaction | Reaction |  |  |  |
| 2 | N4 | Reaction | Reaction | Reaction |  |  |  |
| 3 | N10 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 4 | N9 | Reaction | Reaction | Reaction | Reaction | Reaction | Reaction |
| 5 | N9A | Reaction | Reaction | Reaction |  |  |  |
| 6 | N11A | Reaction | Reaction | Reaction |  |  |  |

## Hot Rolled Steel Properties

|  | Label | E [ksi] | G [ksi] | Nu | Therm. Co.. | Density [k/ft $\left.{ }^{3}\right]$ | Yield [ksi] | Ry | Fu [k | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A992 | 29000 | 11154 | 0.3 | 0.65 | 0.49 | 50 | 1.1 | 65 | 1.1 |
| 2 | A36 Gr. 36 | 29000 | 11154 | 0.3 | 0.65 | 0.49 | 36 | 1.5 | 58 | 1.2 |
| 3 | A572 Gr. 50 | 29000 | 11154 | 0.3 | 0.65 | 0.49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B... | 29000 | 11154 | 0.3 | 0.65 | 0.527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B... | 29000 | 11154 | 0.3 | 0.65 | 0.527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | 0.3 | 0.65 | 0.49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | 0.3 | 0.65 | 0.49 | 50 | 1.4 | 65 | 1.3 |
| 8 | A913 Gr. 65 | 29000 | 11154 | 0.3 | 0.65 | 0.49 | 65 | 1.1 | 80 | 1.1 |

## Primary Member Properties

|  | Label | I Node | J Node | K Node | Rotate(deg) | Section/Sh... | Type | Design List | Material | Design Rule |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | N4 | N11 |  |  | W4X13 | Beam | Wide Flange | A992 | Typical |
| 2 | M2 | N3 | N12 |  |  | W4X13 | Beam | Wide Flange | A992 | Typical |
| 3 | M5 | N9 | N6 |  |  | PIPE_3.5X | Column | Tube | A992 | Typical |
| 4 | M6 | N10 | N5 |  |  | PIPE_3.5X | Column | Tube | A992 | Typical |
| 5 | M5A | N12 | N11 |  |  | 2X8 | Beam | Rectangular | DF | Typical |
| 6 | M6A | N3 | N4 |  |  | 2X8 | Beam | Rectangular | DF | Typical |
| 7 | M7 | N6 | N5 |  |  | W6X25 | Beam | Wide Flange | A992 | Typical |
| 8 | M8 | N9A | N10A |  |  | W4X13 | Beam | Wide Flange | A992 | Typical |
| 9 | M9 | N11A | N12A |  |  | W4X13 | Beam | Wide Flange | A992 | Typical |

## Advanced Member Properties

|  | Label | I Release | $J$ Release | I Offset [in] | J Offset [in] | T/C Only | Physical | Deflection... | Analysis... | Activation | Seismic DR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 |  |  |  |  |  | Yes |  |  |  | None |
| 2 | M2 |  |  |  |  |  | Yes |  |  |  | None |
| 3 | M5 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 4 | M6 |  |  |  |  |  | Yes | ** NA ** |  |  | None |
| 5 | M5A | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 6 | M6A | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 7 | M7 | BenPIN | BenPIN |  |  |  | Yes |  |  |  | None |
| 8 | M8 |  |  |  |  |  | Yes |  |  |  | None |
| 9 | M9 |  |  |  |  |  | Yes |  |  |  | None |

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## Hot Rolled Member Properties

|  | Label | Shape | Length [ft] | Lb y-y [ft] | Lb z-z [ft] | Lcomp t... | Lcomp b...L | L-Torque... | K y-y | K z-z | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | W4X13 | 12.262 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 2 | M2 | W4X13 | 12.262 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 3 | M5 | PIPE_3.5X | 7.5 |  |  |  |  |  |  |  |  | Lateral |
| 4 | M6 | PIPE_3.5X | 7.5 |  |  |  |  |  |  |  |  | Lateral |
| 5 | M7 | W6X25 | 14.4 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 6 | M8 | W4X13 | 12.262 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 7 | M9 | W4X13 | 12.262 |  |  | Lbyy |  |  |  |  |  | Lateral |

Member Distributed Loads (BLC 4 : BLC 1 Transient Area Loads)

|  | ber L | Direction | Start Magnitude.. | End Magnitude... | Start Location [(. | End Location [(f. | Inactive [(k, k-ft)... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Y | -0.029 | -0.029 | 0 | 2.044 | Active |
| 2 | M1 | Y | -0.029 | -0.029 | 2.044 | 4.087 | Active |
| 3 | M1 | Y | -0.029 | -0.029 | 4.087 | 6.131 | Active |
| 4 | M1 | Y | -0.029 | -0.029 | 6.131 | 8.175 | Active |
| 5 | M1 | Y | -0.029 | -0.031 | 8.175 | 10.218 | Active |
| 6 | M1 | Y | -0.031 | -0.036 | 10.218 | 12.262 | Active |
| 7 | M2 | Y | -0.029 | -0.029 | 0 | 2.044 | Active |
| 8 | M2 | Y | -0.029 | -0.029 | 2.044 | 4.087 | Active |
| 9 | M2 | Y | -0.029 | -0.029 | 4.087 | 6.131 | Active |
| 10 | M2 | Y | -0.029 | -0.029 | 6.131 | 8.175 | Active |
| 11 | M2 | Y | -0.029 | -0.031 | 8.175 | 10.218 | Active |
| 12 | M2 | Y | -0.031 | -0.036 | 10.218 | 12.262 | Active |
| 13 | M8 | Y | -0.075 | -0.075 | 0 | 2.044 | Active |
| 14 | M8 | Y | -0.075 | -0.075 | 2.044 | 4.087 | Active |
| 15 | M8 | Y | -0.075 | -0.075 | 4.087 | 6.131 | Active |
| 16 | M8 | Y | -0.075 | -0.075 | 6.131 | 8.175 | Active |
| 17 | M8 | Y | -0.075 | -0.082 | 8.175 | 10.218 | Active |
| 18 | M8 | Y | -0.082 | -0.094 | 10.218 | 12.262 | Active |
| 19 | M9 | Y | -0.075 | -0.075 | 0 | 2.044 | Active |
| 20 | M9 | Y | -0.075 | -0.075 | 2.044 | 4.087 | Active |
| 21 | M9 | Y | -0.075 | -0.075 | 4.087 | 6.131 | Active |
| 22 | M9 | Y | -0.075 | -0.075 | 6.131 | 8.175 | Active |
| 23 | M9 | Y | -0.075 | -0.082 | 8.175 | 10.218 | Active |
| 24 | M9 | Y | -0.082 | -0.094 | 10.218 | 12.262 | Active |

## Member Distributed Loads (BLC 5 : BLC 2 Transient Area Loads)

| Member Label Direction |  |  | Start Magnitude... End Magnitude... Start Location [(... End Location [(f... Inactive [(k, k-ft)... |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | Y | -0.058 | -0.058 | 0 | 2.044 | Active |
| 2 | M1 | Y | -0.058 | -0.058 | 2.044 | 4.087 | Active |
| 3 | M1 | Y | -0.058 | -0.058 | 4.087 | 6.131 | Active |
| 4 | M1 | Y | -0.058 | -0.058 | 6.131 | 8.175 | Active |
| 5 | M1 | Y | -0.058 | -0.063 | 8.175 | 10.218 | Active |
| 6 | M1 | Y | -0.063 | -0.072 | 10.218 | 12.262 | Active |
| 7 | M2 | Y | -0.058 | -0.058 | 0 | 2.044 | Active |
| 8 | M2 | Y | -0.058 | -0.058 | 2.044 | 4.087 | Active |
| 9 | M2 | Y | -0.058 | -0.058 | 4.087 | 6.131 | Active |
| 10 | M2 | Y | -0.058 | -0.058 | 6.131 | 8.175 | Active |
| 11 | M2 | Y | -0.058 | -0.063 | 8.175 | 10.218 | Active |
| 12 | M2 | Y | -0.063 | -0.072 | 10.218 | 12.262 | Active |
| 13 | M8 | Y | -0.151 | -0.151 | 0 | 2.044 | Active |
| 14 | M8 | Y | -0.151 | -0.151 | 2.044 | 4.087 | Active |
| 15 | M8 | Y | -0.151 | -0.151 | 4.087 | 6.131 | Active |
| 16 | M8 | Y | -0.151 | -0.151 | 6.131 | 8.175 | Active |
| 17 | M8 | Y | -0.151 | -0.163 | 8.175 | 10.218 | Active |
| 18 | M8 | Y | -0.163 | -0.188 | 10.218 | 12.262 | Active |
| 19 | M9 | Y | -0.151 | -0.151 | 0 | 2.044 | Active |
| 20 | M9 | Y | -0.151 | -0.151 | 2.044 | 4.087 | Active |
| 21 | M9 | Y | -0.151 | -0.151 | 4.087 | 6.131 | Active |
| 22 | M9 | Y | -0.151 | -0.151 | 6.131 | 8.175 | Active |
| 23 | M9 | Y | -0.151 | -0.163 | 8.175 | 10.218 | Active |
| 24 | M9 | Y | -0.163 | -0.188 | 10.218 | 12.262 | Active |

## Basic Load Cases

|  | BLC Descr... | Category | X Gravity | Y Gravity | Z Gravity | Nodal | Point | Distributed | Area(Mem.. | Surface(PI... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | D | DL |  | -1 |  |  |  |  | 1 |  |
| 2 | S | SL |  |  |  |  |  |  | 1 |  |
| 3 | E | EL |  |  |  |  |  |  |  |  |
| 4 | BLC 1 Tra... | None |  |  |  |  |  | 24 |  |  |
| 5 | BLC 2 Tra... | None |  |  |  |  |  | 24 |  |  |

## Load Combinations

| 1 | D | Yes | Y | 1 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | S | Yes | Y | 2 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | D+S | Yes | Y | 1 | 1 | 2 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Load Combination Design

| Description ASIF   <br> 1 D  |  |  | Service | Hot Rolled | Cold For.. | Wood | Concrete | Masonry | Aluminum | Stainless | Connecti... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 2 | S |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| 3 | D+S |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |

## Member Section Forces

|  | LC | Member Label | Sec | Axial [k] | y Shear [k] | z Shear [k] | Torque [k-ft] | y-y Momen | z-z Moment... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | 1 | 0.018 | 0.17 | 0 | 0 | 0 | -0.015 |
| 2 |  |  | 2 | 0.005 | 0.042 | 0 | 0 | 0 | -0.339 |
| 3 |  |  | 3 | -0.008 | -0.086 | 0 | 0 | 0 | -0.271 |
| 4 |  |  | 4 | -0.021 | -0.215 | 0 | 0 | 0 | 0.191 |
| 5 |  |  | 5 | 0.005 | 0.047 | 0 | 0 | 0 | -0.005 |
| 6 | 1 | M2 | 1 | 0.018 | 0.17 | 0 | 0 | 0 | -0.015 |
| 7 |  |  | 2 | 0.005 | 0.042 | 0 | 0 | 0 | -0.339 |
| 8 |  |  | 3 | -0.008 | -0.086 | 0 | 0 | 0 | -0.271 |
| 9 |  |  | 4 | -0.021 | -0.215 | 0 | 0 | 0 | 0.191 |
| 10 |  |  | 5 | 0.005 | 0.047 | 0 | 0 | 0 | -0.005 |
| 11 | 1 | M5 | 1 | 1.337 | 0 | -0.028 | 0 | 0.071 | 0 |
| 12 |  |  | 2 | 1.315 | 0 | -0.028 | 0 | 0.018 | 0 |
| 13 |  |  | 3 | 1.293 | 0 | -0.028 | 0 | -0.035 | 0 |
| 14 |  |  | 4 | 1.271 | 0 | -0.028 | 0 | -0.089 | 0 |
| 15 |  |  | 5 | 1.249 | 0 | -0.028 | 0 | -0.142 | 0 |
| 16 | 1 | M6 | 1 | 1.337 | 0 | -0.028 | 0 | 0.071 | 0 |
| 17 |  |  | 2 | 1.315 | 0 | -0.028 | 0 | 0.018 | 0 |
| 18 |  |  | 3 | 1.293 | 0 | -0.028 | 0 | -0.035 | 0 |
| 19 |  |  | 4 | 1.271 | 0 | -0.028 | 0 | -0.089 | 0 |
| 20 |  |  | 5 | 1.249 | 0 | -0.028 | 0 | -0.142 | 0 |
| 21 | 1 | M5A | 1 | 0 | 0.047 | 0 | 0.005 | 0 | 0 |
| 22 |  |  | 2 | 0 | 0.037 | 0 | 0.005 | 0 | -0.151 |
| 23 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | -0.181 |
| 24 |  |  | 4 | 0 | -0.037 | 0 | -0.005 | 0 | -0.151 |
| 25 |  |  | 5 | 0 | -0.047 | 0 | -0.005 | 0 | 0 |
| 26 | 1 | M6A | 1 | 0 | 0.003 | 0 | -0.015 | 0 | 0 |
| 27 |  |  | 2 | 0 | -0.007 | 0 | -0.015 | 0 | 0.006 |
| 28 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | -0.006 |
| 29 |  |  | 4 | 0 | 0.007 | 0 | 0.015 | 0 | 0.006 |
| 30 |  |  | 5 | 0 | -0.003 | 0 | 0.015 | 0 | 0 |
| 31 | 1 | M7 | 1 | 0 | 0.846 | 0.027 | -0.005 | 0 | 0 |
| 32 |  |  | 2 | 0 | 0.756 | 0.027 | -0.005 | 0.098 | -2.883 |
| 33 |  |  | 3 | 0 | 0 | 0 | 0 | 0.107 | -3.308 |
| 34 |  |  | 4 | 0 | -0.756 | -0.027 | 0.005 | 0.098 | -2.883 |
| 35 |  |  | 5 | 0 | -0.846 | -0.027 | 0.005 | 0 | 0 |
| 36 | 1 | M8 | 1 | 0.07 | 0.418 | 0 | 0.002 | 0 | 0.015 |
| 37 |  |  | 2 | 0.042 | 0.148 | 0 | 0.002 | 0 | -0.852 |
| 38 |  |  | 3 | 0.015 | -0.122 | 0 | 0.002 | 0 | -0.892 |
| 39 |  |  | 4 | -0.012 | -0.393 | 0 | 0.002 | 0 | -0.104 |
| 40 |  |  | 5 | -0.003 | -0.028 | 0 | -0.001 | 0 | 0.005 |

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## Member Section Forces (Continued)

|  | LC | Member Label | Sec | Axial [k] | y Shear [k] | z Shear [k] | Torque [k-ft] | y-y Momen | z-z Moment... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 1 | M9 | 1 | 0.07 | 0.418 | 0 | -0.002 | 0 | 0.015 |
| 42 |  |  | 2 | 0.042 | 0.148 | 0 | -0.002 | 0 | -0.852 |
| 43 |  |  | 3 | 0.015 | -0.122 | 0 | -0.002 | 0 | -0.892 |
| 44 |  |  | 4 | -0.012 | -0.393 | 0 | -0.002 | 0 | -0.104 |
| 45 |  |  | 5 | -0.003 | -0.028 | 0 | 0.001 | 0 | 0.005 |
| 46 | 2 | M1 | 1 | 0.027 | 0.235 | 0 | 0 | 0 | -0.025 |
| 47 |  |  | 2 | 0.01 | 0.058 | 0 | 0 | 0 | -0.475 |
| 48 |  |  | 3 | -0.008 | -0.119 | 0 | 0 | 0 | -0.384 |
| 49 |  |  | 4 | -0.026 | -0.297 | 0 | 0 | 0 | 0.251 |
| 50 |  |  | 5 | 0.005 | 0.053 | 0 | 0 | 0 | -0.01 |
| 51 | 2 | M2 | 1 | 0.027 | 0.235 | 0 | 0 | 0 | -0.025 |
| 52 |  |  | 2 | 0.01 | 0.058 | 0 | 0 | 0 | -0.475 |
| 53 |  |  | 3 | -0.008 | -0.119 | 0 | 0 | 0 | -0.384 |
| 54 |  |  | 4 | -0.026 | -0.297 | 0 | 0 | 0 | 0.251 |
| 55 |  |  | 5 | 0.005 | 0.053 | 0 | 0 | 0 | -0.01 |
| 56 | 2 | M5 | 1 | 1.692 | 0 | -0.042 | 0 | 0.105 | 0 |
| 57 |  |  | 2 | 1.692 | 0 | -0.042 | 0 | 0.026 | 0 |
| 58 |  |  | 3 | 1.692 | 0 | -0.042 | 0 | -0.052 | 0 |
| 59 |  |  | 4 | 1.692 | 0 | -0.042 | 0 | -0.131 | 0 |
| 60 |  |  | 5 | 1.692 | 0 | -0.042 | 0 | -0.209 | 0 |
| 61 | 2 | M6 | 1 | 1.692 | 0 | -0.042 | 0 | 0.105 | 0 |
| 62 |  |  | 2 | 1.692 | 0 | -0.042 | 0 | 0.026 | 0 |
| 63 |  |  | 3 | 1.692 | 0 | -0.042 | 0 | -0.052 | 0 |
| 64 |  |  | 4 | 1.692 | 0 | -0.042 | 0 | -0.131 | 0 |
| 65 |  |  | 5 | 1.692 | 0 | -0.042 | 0 | -0.209 | 0 |
| 66 | 2 | M5A | 1 | 0 | 0.053 | 0 | 0.01 | 0 | 0 |
| 67 |  |  | 2 | 0 | 0.053 | 0 | 0.01 | 0 | -0.191 |
| 68 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | -0.215 |
| 69 |  |  | 4 | 0 | -0.053 | 0 | -0.01 | 0 | -0.191 |
| 70 |  |  | 5 | 0 | -0.053 | 0 | -0.01 | 0 | 0 |
| 71 | 2 | M6A | 1 | 0 | 0 | 0 | -0.025 | 0 | 0 |
| 72 |  |  | 2 | 0 | 0 | 0 | -0.025 | 0 | 0.002 |
| 73 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 74 |  |  | 4 | 0 | 0 | 0 | 0.025 | 0 | 0.002 |
| 75 |  |  | 5 | 0 | 0 | 0 | 0.025 | 0 | 0 |
| 76 | 2 | M7 | 1 | 0 | 1.14 | 0.038 | -0.011 | 0 | 0 |
| 77 |  |  | 2 | 0 | 1.14 | 0.038 | -0.011 | 0.137 | -4.104 |
| 78 |  |  | 3 | 0 | 0 | 0 | 0 | 0.149 | -4.555 |
| 79 |  |  | 4 | 0 | -1.14 | -0.038 | 0.011 | 0.137 | -4.104 |
| 80 |  |  | 5 | 0 | -1.14 | -0.038 | 0.011 | 0 | 0 |
| 81 | 2 | M8 | 1 | 0.11 | 0.712 | 0 | 0.003 | 0 | 0.025 |
| 82 |  |  | 2 | 0.064 | 0.252 | 0 | 0.003 | 0 | -1.453 |
| 83 |  |  | 3 | 0.017 | -0.208 | 0 | 0.003 | 0 | -1.521 |
| 84 |  |  | 4 | -0.029 | -0.671 | 0 | 0.003 | 0 | -0.177 |
| 85 |  |  | 5 | -0.005 | -0.053 | 0 | -0.003 | 0 | 0.01 |
| 86 | 2 | M9 | 1 | 0.11 | 0.712 | 0 | -0.003 | 0 | 0.025 |
| 87 |  |  | 2 | 0.064 | 0.252 | 0 | -0.003 | 0 | -1.453 |
| 88 |  |  | 3 | 0.017 | -0.208 | 0 | -0.003 | 0 | -1.521 |
| 89 |  |  | 4 | -0.029 | -0.671 | 0 | -0.003 | 0 | -0.177 |
| 90 |  |  | 5 | -0.005 | -0.053 | 0 | 0.003 | 0 | 0.01 |
| 91 | 3 | M1 | 1 | 0.046 | 0.406 | 0 | 0 | 0 | -0.04 |
| 92 |  |  | 2 | 0.015 | 0.1 | 0 | 0 | 0 | -0.815 |
| 93 |  |  | 3 | -0.016 | -0.205 | 0 | 0 | 0 | -0.655 |
| 94 |  |  | 4 | -0.047 | -0.512 | 0 | 0 | 0 | 0.442 |
| 95 |  |  | 5 | 0.01 | 0.099 | 0 | 0 | 0 | -0.015 |
| 96 | 3 | M2 | 1 | 0.046 | 0.406 | 0 | 0 | 0 | -0.04 |
| 97 |  |  | 2 | 0.015 | 0.1 | 0 | 0 | 0 | -0.815 |
| 98 |  |  | 3 | -0.016 | -0.205 | 0 | 0 | 0 | -0.655 |
| 99 |  |  | 4 | -0.047 | -0.512 | 0 | 0 | 0 | 0.442 |
| 100 |  |  | 5 | 0.01 | 0.099 | 0 | 0 | 0 | -0.015 |
| 101 | 3 | M5 | 1 | 3.028 | 0 | -0.07 | 0 | 0.176 | 0 |
| 102 |  |  | 2 | 3.007 | 0 | -0.07 | 0 | 0.044 | 0 |


|  | LC | Member Label | Sec | Axial [k] | y Shear [k] | z Shear [k] | Torque [k-ft] | y-y Momen | Moment... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 103 |  |  | 3 | 2.985 | 0 | -0.07 | 0 | -0.088 | 0 |
| 104 |  |  | 4 | 2.963 | 0 | -0.07 | 0 | -0.219 | 0 |
| 105 |  |  | 5 | 2.941 | 0 | -0.07 | 0 | -0.351 | 0 |
| 106 | 3 | M6 | 1 | 3.028 | 0 | -0.07 | 0 | 0.176 | 0 |
| 107 |  |  | 2 | 3.007 | 0 | -0.07 | 0 | 0.044 | 0 |
| 108 |  |  | 3 | 2.985 | 0 | -0.07 | 0 | -0.088 | 0 |
| 109 |  |  | 4 | 2.963 | 0 | -0.07 | 0 | -0.219 | 0 |
| 110 |  |  | 5 | 2.941 | 0 | -0.07 | 0 | -0.351 | 0 |
| 111 | 3 | M5A | 1 | 0 | 0.1 | 0 | 0.015 | 0 | 0 |
| 112 |  |  | 2 | 0 | 0.09 | 0 | 0.015 | -0.002 | -0.342 |
| 113 |  |  | 3 | -0.001 | 0 | 0 | 0 | -0.002 | -0.396 |
| 114 |  |  | 4 | 0 | -0.09 | 0 | -0.015 | -0.002 | -0.342 |
| 115 |  |  | 5 | 0 | -0.1 | 0 | -0.015 | 0 | 0 |
| 116 | 3 | M6A | 1 | 0 | 0.003 | 0 | -0.04 | 0 | 0 |
| 117 |  |  | 2 | 0 | -0.007 | 0 | -0.04 | 0 | 0.008 |
| 118 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | -0.007 |
| 119 |  |  | 4 | 0 | 0.007 | 0 | 0.04 | 0 | 0.008 |
| 120 |  |  | 5 | 0 | -0.003 | 0 | 0.04 | 0 | 0 |
| 121 | 3 | M7 | 1 | 0 | 1.986 | 0.065 | -0.016 | 0 | 0 |
| 122 |  |  | 2 | 0 | 1.896 | 0.065 | -0.016 | 0.234 | -6.987 |
| 123 |  |  | 3 | 0.001 | 0 | 0 | 0 | 0.256 | -7.863 |
| 124 |  |  | 4 | 0 | -1.896 | -0.065 | 0.016 | 0.234 | -6.987 |
| 125 |  |  | 5 | 0 | -1.986 | -0.065 | 0.016 | 0 | 0 |
| 126 | 3 | M8 | 1 | 0.18 | 1.13 | 0 | 0.004 | 0 | 0.04 |
| 127 |  |  | 2 | 0.106 | 0.4 | 0 | 0.004 | 0 | -2.306 |
| 128 |  |  | 3 | 0.033 | -0.33 | 0 | 0.004 | 0 | -2.413 |
| 129 |  |  | 4 | -0.042 | -1.065 | 0 | 0.004 | 0 | -0.281 |
| 130 |  |  | 5 | -0.008 | -0.08 | 0.001 | -0.004 | 0 | 0.015 |
| 131 | 3 | M9 | 1 | 0.18 | 1.13 | 0 | -0.004 | 0 | 0.04 |
| 132 |  |  | 2 | 0.106 | 0.4 | 0 | -0.004 | 0 | -2.306 |
| 133 |  |  | 3 | 0.033 | -0.33 | 0 | -0.004 | 0 | -2.413 |
| 134 |  |  | 4 | -0.042 | -1.065 | 0 | -0.004 | 0 | -0.281 |
| 135 |  |  | 5 | -0.008 | -0.08 | -0.001 | 0.004 | 0 | 0.015 |

## Maximum Member Section Forces

| LC Me |  |  |  | Axial [k] | $\frac{\operatorname{Loc}[f t]}{0}$ | y She... | Loc [ft] z She... |  | Loc [ft] | Torque... |  | y-y Mo... Loc [ft] |  | z-z Mo... Loc [ft] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | max | 0.018 |  | 0.17 | 0 | 0 | 12.262 | 0 | 12.262 | 0 | 12.262 | 0.337 | 9.835 |
| 2 |  |  | min | -0.023 | 9.835 | -0.243 | 9.835 | 0 | 0 | 0 | 0 | 0 | 9.963 | -0.36 | 4.087 |
| 3 | 1 | M2 | max | 0.018 | 0 | 0.17 | 0 | 0 | 9.835 | 0 | 12.262 | 0 | 9.963 | 0.337 | 9.835 |
| 4 |  |  | min | -0.023 | 9.835 | -0.243 | 9.835 | 0 | 9.963 | 0 | 0 | 0 | 0 | -0.36 | 4.087 |
| 5 | 1 | M5 | max | 1.337 | 0 | 0 | 7.5 | -0.028 | 7.5 | 0 | 7.5 | 0.071 | 0 | 0 | 7.5 |
| 6 |  |  | min | 1.249 | 7.5 | 0 | 0 | -0.028 | 0 | 0 | 0 | -0.142 | 7.5 | 0 | 0 |
| 7 | 1 | M6 | max | 1.337 | 0 | 0 | 7.5 | -0.028 | 7.5 | 0 | 7.5 | 0.071 | 0 | 0 | 0 |
| 8 |  |  | min | 1.249 | 7.5 | 0 | 0 | -0.028 | 0 | 0 | 0 | -0.142 | 7.5 | 0 | 7.5 |
| 9 | 1 | M5A | max | 0 | 14.4 | 0.047 | 0 | 0 | 14.4 | 0.005 | 3.9 | 0 | 14.4 | 0 | 14.4 |
| 10 |  |  | min | 0 | 4.05 | -0.047 | 14.4 | 0 | 0 | -0.005 | 10.5 | 0 | 4.05 | -0.181 | 7.2 |
| 11 | 1 | M6A | max | 0 | 14.4 | 0.008 | 4.05 | 0 | 3.9 | 0.015 | 14.4 | 0 | 3.9 | 0.008 | 10.5 |
| 12 |  |  | min | 0 | 0 | -0.008 | 10.35 | 0 | 10.5 | -0.015 | 0 | 0 | 4.05 | -0.006 | 7.2 |
| 13 | 1 | M7 | max | 0 | 10.35 | 0.846 | 0 | 0.027 | 3.9 | 0.005 | 14.4 | 0.107 | 10.35 | 0 | 14.4 |
| 14 |  |  | min | 0 | 0 | -0.846 | 14.4 | -0.027 | 10.5 | -0.005 | 0 | 0 | 0 | -3.308 | 7.2 |
| 15 | 1 | M8 | max | 0.07 | 0 | 0.418 | 0 | 0 | 12.262 | 0.002 | 9.835 | 0 | 9.835 | 0.21 | 9.963 |
| 16 |  |  | min | -0.018 | 9.835 | -0.452 | 9.835 | 0 | 0 | -0.001 | 9.963 | -0.001 | 9.963 | -0.977 | 4.726 |
| 17 | 1 | M9 | max | 0.07 | 0 | 0.418 | 0 | 0 | 9.835 | 0.001 | 12.262 | 0.001 | 9.963 | 0.21 | 9.963 |
| 18 |  |  | min | -0.018 | 9.835 | -0.452 | 9.835 | 0 | 9.963 | -0.002 | 0 | 0 | 9.835 | -0.977 | 4.726 |
| 19 | 2 | M1 | max | 0.027 | 0 | 0.235 | 0 | 0 | 12.262 | 0 | 12.262 | 0 | 12.262 | 0.453 | 9.835 |
| 20 |  |  | min | -0.03 | 9.835 | -0.336 | 9.835 | 0 | 0 | 0 | 0 | 0 | 9.963 | -0.505 | 4.087 |
| 21 | 2 | M2 | max | 0.027 | 0 | 0.235 | 0 | 0 | 9.835 | 0 | 12.262 | 0 | 9.963 | 0.453 | 9.835 |
| 22 |  |  | min | -0.03 | 9.835 | -0.336 | 9.835 | 0 | 9.963 | 0 | 0 | 0 | 0 | -0.505 | 4.087 |
| 23 | 2 | M5 | max | 1.692 | 7.5 | 0 | 7.5 | -0.042 | 7.5 | 0 | 7.5 | 0.105 | 0 | 0 | 7.5 |
| 24 |  |  | min | 1.692 | 0 | 0 | 0 | -0.042 | 0 | 0 | 0 | -0.209 | 7.5 | 0 | 0 |
| 25 | 2 | M6 | max | 1.692 | 7.5 | 0 | 7.5 | -0.042 | 7.5 | 0 | 7.5 | 0.105 | 0 | 0 | 0 |

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## Maximum Member Section Forces (Continued)

LC Memb..

| LC | Memb... |  |  |
| :---: | :---: | :---: | :---: |
| 26 |  |  |  |
| 27 | 2 | M5A |  |
| 28 |  |  |  |
| 29 | 2 | M6A |  |
| 30 |  |  |  |
| 31 | 2 | M7 |  |
| 32 |  |  |  |
| 33 | 2 | M8 |  |
| 34 |  |  |  |
| 35 | 2 | M9 |  |
| 36 |  |  |  |
| 37 | 3 | M1 |  |
| 38 |  |  |  |
| 39 | 3 | M2 |  |
| 40 |  |  |  |
| 41 | 3 | M5 |  |
| 42 |  |  |  |
| 43 | 3 | M6 |  |
| 44 |  |  |  |
| 45 | 3 | M5A |  |
| 46 |  |  |  |
| 47 | 3 | M6A |  |
| 48 |  |  |  |
| 49 | 3 | M7 |  |
| 50 |  |  |  |
| 51 | 3 | M8 |  |
| 52 |  |  |  |
| 53 | 3 | M9 |  |
| 54 |  |  |  |

Axial [k] Loc [ft] y She... Loc [ft] z She... Loc [ft] Torque... Loc [ft] y-y Mo... Loc [ft] z-z Mo... Loc [ft]

## Member End Reactions

|  | LC | Member Label | Member End | Axial [k] | y Shear [k] | z Shear [k] | Torque [k-ft] | y-y Momen | z-z Moment... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | I | 0.018 | 0.17 | 0 | 0 | 0 | -0.015 |
| 2 |  |  | $J$ | 0.005 | 0.047 | 0 | 0 | 0 | -0.005 |
| 3 | 1 | M2 | I | 0.018 | 0.17 | 0 | 0 | 0 | -0.015 |
| 4 |  |  | $J$ | 0.005 | 0.047 | 0 | 0 | 0 | -0.005 |
| 5 | 1 | M5 | I | 1.337 | 0 | -0.028 | 0 | 0.071 | 0 |
| 6 |  |  | $J$ | 1.249 | 0 | -0.028 | 0 | -0.142 | 0 |
| 7 | 1 | M6 | I | 1.337 | 0 | -0.028 | 0 | 0.071 | 0 |
| 8 |  |  | $J$ | 1.249 | 0 | -0.028 | 0 | -0.142 | 0 |
| 9 | 1 | M5A | I | 0 | 0.047 | 0 | 0.005 | 0 | 0 |
| 10 |  |  | $J$ | 0 | -0.047 | 0 | -0.005 | 0 | 0 |
| 11 | 1 | M6A | I | 0 | 0.003 | 0 | -0.015 | 0 | 0 |
| 12 |  |  | $J$ | 0 | -0.003 | 0 | 0.015 | 0 | 0 |
| 13 | 1 | M7 | I | 0 | 0.846 | 0.027 | -0.005 | 0 | 0 |
| 14 |  |  | $J$ | 0 | -0.846 | -0.027 | 0.005 | 0 | 0 |
| 15 | 1 | M8 | 1 | 0.07 | 0.418 | 0 | 0.002 | 0 | 0.015 |
| 16 |  |  | $J$ | -0.003 | -0.028 | 0 | -0.001 | 0 | 0.005 |
| 17 | 1 | M9 | I | 0.07 | 0.418 | 0 | -0.002 | 0 | 0.015 |
| 18 |  |  | $J$ | -0.003 | -0.028 | 0 | 0.001 | 0 | 0.005 |
| 19 | 2 | M1 | 1 | 0.027 | 0.235 | 0 | 0 | 0 | -0.025 |
| 20 |  |  | $J$ | 0.005 | 0.053 | 0 | 0 | 0 | -0.01 |
| 21 | 2 | M2 | I | 0.027 | 0.235 | 0 | 0 | 0 | -0.025 |
| 22 |  |  | $J$ | 0.005 | 0.053 | 0 | 0 | 0 | -0.01 |
| 23 | 2 | M5 | 1 | 1.692 | 0 | -0.042 | 0 | 0.105 | 0 |
| 24 |  |  | J | 1.692 | 0 | -0.042 | 0 | -0.209 | 0 |
| 25 | 2 | M6 | 1 | 1.692 | 0 | -0.042 | 0 | 0.105 | 0 |
| 26 |  |  | J | 1.692 | 0 | -0.042 | 0 | -0.209 | 0 |
| 27 | 2 | M5A | 1 | 0 | 0.053 | 0 | 0.01 | 0 | 0 |
| 28 |  |  | J | 0 | -0.053 | 0 | -0.01 | 0 | 0 |
| 29 | 2 | M6A | 1 | 0 | 0 | 0 | -0.025 | 0 | 0 |

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## Member End Reactions (Continued)

|  | LC | Member Label | Member End | Axial [k] | y Shear [k] | z Shear [k] | Torque [k-ft] | y-y Momen | z Moment... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 |  |  | J | 0 | 0 | 0 | 0.025 | 0 | 0 |
| 31 | 2 | M7 | I | 0 | 1.14 | 0.038 | -0.011 | 0 | 0 |
| 32 |  |  | $J$ | 0 | -1.14 | -0.038 | 0.011 | 0 | 0 |
| 33 | 2 | M8 | , | 0.11 | 0.712 | 0 | 0.003 | 0 | 0.025 |
| 34 |  |  | J | -0.005 | -0.053 | 0 | -0.003 | 0 | 0.01 |
| 35 | 2 | M9 | , | 0.11 | 0.712 | 0 | -0.003 | 0 | 0.025 |
| 36 |  |  | J | -0.005 | -0.053 | 0 | 0.003 | 0 | 0.01 |
| 37 | 3 | M1 | 1 | 0.046 | 0.406 | 0 | 0 | 0 | -0.04 |
| 38 |  |  | J | 0.01 | 0.099 | 0 | 0 | 0 | -0.015 |
| 39 | 3 | M2 | 1 | 0.046 | 0.406 | 0 | 0 | 0 | -0.04 |
| 40 |  |  | $J$ | 0.01 | 0.099 | 0 | 0 | 0 | -0.015 |
| 41 | 3 | M5 | I | 3.028 | 0 | -0.07 | 0 | 0.176 | 0 |
| 42 |  |  | $J$ | 2.941 | 0 | -0.07 | 0 | -0.351 | 0 |
| 43 | 3 | M6 | I | 3.028 | 0 | -0.07 | 0 | 0.176 | 0 |
| 44 |  |  | $J$ | 2.941 | 0 | -0.07 | 0 | -0.351 | 0 |
| 45 | 3 | M5A | I | 0 | 0.1 | 0 | 0.015 | 0 | 0 |
| 46 |  |  | J | 0 | -0.1 | 0 | -0.015 | 0 | 0 |
| 47 | 3 | M6A | I | 0 | 0.003 | 0 | -0.04 | 0 | 0 |
| 48 |  |  | J | 0 | -0.003 | 0 | 0.04 | 0 | 0 |
| 49 | 3 | M7 | 1 | 0 | 1.986 | 0.065 | -0.016 | 0 | 0 |
| 50 |  |  | J | 0 | -1.986 | -0.065 | 0.016 | 0 | 0 |
| 51 | 3 | M8 | I | 0.18 | 1.13 | 0 | 0.004 | 0 | 0.04 |
| 52 |  |  | $J$ | -0.008 | -0.08 | 0.001 | -0.004 | 0 | 0.015 |
| 53 | 3 | M9 | 1 | 0.18 | 1.13 | 0 | -0.004 | 0 | 0.04 |
| 54 |  |  | J | -0.008 | -0.08 | -0.001 | 0.004 | 0 | 0.015 |

## Torsion

|  | LC | Member Label | Sec | Torque [k-ft] | Shear [ksi] | y Warp She... | z Warp She... | z-Top Warp... | z-Bot Warp... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2 |  |  | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4 |  |  | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5 |  |  | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6 | 1 | M2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7 |  |  | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9 |  |  | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10 |  |  | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11 | 1 | M5 | 1 | 0 | 0 | NC | NC | NC | NC |
| 12 |  |  | 2 | 0 | 0 | NC | NC | NC | NC |
| 13 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 14 |  |  | 4 | 0 | 0 | NC | NC | NC | NC |
| 15 |  |  | 5 | 0 | 0 | NC | NC | NC | NC |
| 16 | 1 | M6 | 1 | 0 | 0 | NC | NC | NC | NC |
| 17 |  |  | 2 | 0 | 0 | NC | NC | NC | NC |
| 18 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 19 |  |  | 4 | 0 | 0 | NC | NC | NC | NC |
| 20 |  |  | 5 | 0 | 0 | NC | NC | NC | NC |
| 21 | 1 | M5A | 1 | 0.005 | 0.012 | NC | NC | NC | NC |
| 22 |  |  | 2 | 0.005 | 0.012 | NC | NC | NC | NC |
| 23 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 24 |  |  | 4 | -0.005 | -0.012 | NC | NC | NC | NC |
| 25 |  |  | 5 | -0.005 | -0.012 | NC | NC | NC | NC |
| 26 | 1 | M6A | 1 | -0.015 | -0.037 | NC | NC | NC | NC |
| 27 |  |  | 2 | -0.015 | -0.037 | NC | NC | NC | NC |
| 28 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 29 |  |  | 4 | 0.015 | 0.037 | NC | NC | NC | NC |
| 30 |  |  | 5 | 0.015 | 0.037 | NC | NC | NC | NC |
| 31 | 1 | M7 | 1 | -0.005 | -0.061 | NC | NC | NC | NC |
| 32 |  |  | 2 | -0.005 | -0.061 | NC | NC | NC | NC |
| 33 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |

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## Torsion (Continued)

|  | LC | Member Label | Sec | Torque [k-ft] | Shear [ksi] | y Warp She... z Warp She... z-Top Warp... z-Bot Warp... |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 96 | 3 | M2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 97 |  |  | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 98 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 99 |  |  | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| 100 |  |  | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 101 | 3 | M5 | 1 | 0 | 0 | NC | NC | NC | NC |
| 102 |  |  | 2 | 0 | 0 | NC | NC | NC | NC |
| 103 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 104 |  |  | 4 | 0 | 0 | NC | NC | NC | NC |
| 105 |  |  | 5 | 0 | 0 | NC | NC | NC | NC |
| 106 | 3 | M6 | 1 | 0 | 0 | NC | NC | NC | NC |
| 107 |  |  | 2 | 0 | 0 | NC | NC | NC | NC |
| 108 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 109 |  |  | 4 | 0 | 0 | NC | NC | NC | NC |
| 110 |  |  | 5 | 0 | 0 | NC | NC | NC | NC |
| 111 | 3 | M5A | 1 | 0.015 | 0.038 | NC | NC | NC | NC |
| 112 |  |  | 2 | 0.015 | 0.038 | NC | NC | NC | NC |
| 113 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 114 |  |  | 4 | -0.015 | -0.038 | NC | NC | NC | NC |
| 115 |  |  | 5 | -0.015 | -0.038 | NC | NC | NC | NC |
| 116 | 3 | M6A | 1 | -0.04 | -0.101 | NC | NC | NC | NC |
| 117 |  |  | 2 | -0.04 | -0.101 | NC | NC | NC | NC |
| 118 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 119 |  |  | 4 | 0.04 | 0.101 | NC | NC | NC | NC |
| 120 |  |  | 5 | 0.04 | 0.101 | NC | NC | NC | NC |
| 121 | 3 | M7 | 1 | -0.016 | -0.195 | NC | NC | NC | NC |
| 122 |  |  | 2 | -0.016 | -0.195 | NC | NC | NC | NC |
| 123 |  |  | 3 | 0 | 0 | NC | NC | NC | NC |
| 124 |  |  | 4 | 0.016 | 0.195 | NC | NC | NC | NC |
| 125 |  |  | 5 | 0.016 | 0.195 | NC | NC | NC | NC |
| 126 | 3 | M8 | 1 | 0.004 | 0 | 0 | 0.015 | 0.223 | 0.223 |
| 127 |  |  | 2 | 0.004 | 0.108 | 0 | 0.001 | 0.021 | 0.021 |
| 128 |  |  | 3 | 0.004 | 0.117 | 0 | 0 | 0 | 0 |
| 129 |  |  | 4 | 0.004 | 0.108 | 0 | 0.001 | -0.021 | -0.021 |
| 130 |  |  | 5 | -0.004 | 0 | 0 | -0.015 | 0.227 | 0.227 |
| 131 | 3 | M9 | 1 | -0.004 | 0 | 0 | -0.015 | -0.223 | -0.223 |
| 132 |  |  | 2 | -0.004 | -0.108 | 0 | -0.001 | -0.021 | -0.021 |
| 133 |  |  | 3 | -0.004 | -0.117 | 0 | 0 | 0 | 0 |
| 134 |  |  | 4 | -0.004 | -0.108 | 0 | -0.001 | 0.021 | 0.021 |
| 135 |  |  | 5 | 0.004 | 0 | 0 | 0.015 | -0.227 | -0.227 |

## Member Section Stresses

|  | LC | Member L... | Sec | Axial [ksi] | y Shear [ksi] | z Shear [ksi] | y top Bend. | y bot Bend. | $z$ top Bend. | z bot Bend.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | 1 | 0.005 | 0.146 | 0 | 0.033 | -0.033 | 0 | 0 |
| 2 |  |  | 2 | 0.001 | 0.036 | 0 | 0.75 | -0.75 | 0 | 0 |
| 3 |  |  | 3 | -0.002 | -0.074 | 0 | 0.599 | -0.599 | 0 | 0 |
| 4 |  |  | 4 | -0.005 | -0.185 | 0 | -0.421 | 0.421 | 0 | 0 |
| 5 |  |  | 5 | 0.001 | 0.04 | 0 | 0.011 | -0.011 | 0 | 0 |
| 6 | 1 | M2 | 1 | 0.005 | 0.146 | 0 | 0.033 | -0.033 | 0 | 0 |
| 7 |  |  | 2 | 0.001 | 0.036 | 0 | 0.75 | -0.75 | 0 | 0 |
| 8 |  |  | 3 | -0.002 | -0.074 | 0 | 0.599 | -0.599 | 0 | 0 |
| 9 |  |  | 4 | -0.005 | -0.185 | 0 | -0.421 | 0.421 | 0 | 0 |
| 10 |  |  | 5 | 0.001 | 0.04 | 0 | 0.011 | -0.011 | 0 | 0 |
| 11 | 1 | M5 | 1 | 0.39 | 0 | -0.017 | 0 | 0 | 0.287 | -0.287 |
| 12 |  |  | 2 | 0.383 | 0 | -0.017 | 0 | 0 | 0.072 | -0.072 |
| 13 |  |  | 3 | 0.377 | 0 | -0.017 | 0 | 0 | -0.143 | 0.143 |
| 14 |  |  | 4 | 0.371 | 0 | -0.017 | 0 | 0 | -0.358 | 0.358 |
| 15 |  |  | 5 | 0.364 | 0 | -0.017 | 0 | 0 | -0.573 | 0.573 |
| 16 | 1 | M6 | 1 | 0.39 | 0 | -0.017 | 0 | 0 | 0.287 | -0.287 |
| 17 |  |  | 2 | 0.383 | 0 | -0.017 | 0 | 0 | 0.072 | -0.072 |
| 18 |  |  | 3 | 0.377 | 0 | -0.017 | 0 | 0 | -0.143 | 0.143 |

LC Member L... Sec
Axial [ksi] y Shear [ksi] z Shear [ksi] y top Bend... y bot Bend... z top Bend... z bot Bend. .

| 19 |  |  | 4 | 0.371 | 0 | -0.017 | 0 | 0 | -0.358 | 0.358 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 |  |  | 5 | 0.364 | 0 | -0.017 | 0 | 0 | -0.573 | 0.573 |
| 21 | 1 | M5A | 1 | 0 | 0.006 | 0 | 0 | 0 | 0 | 0 |
| 22 |  |  | 2 | 0 | 0.005 | 0 | 0.138 | -0.138 | -0.003 | 0.003 |
| 23 |  |  | 3 | 0 | 0 | 0 | 0.165 | -0.165 | -0.003 | 0.003 |
| 24 |  |  | 4 | 0 | -0.005 | 0 | 0.138 | -0.138 | -0.003 | 0.003 |
| 25 |  |  | 5 | 0 | -0.006 | 0 | 0 | 0 | 0 | 0 |
| 26 | 1 | M6A | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 27 |  |  | 2 | 0 | 0 | 0 | -0.006 | 0.006 | 0 | 0 |
| 28 |  |  | 3 | 0 | 0 | 0 | 0.006 | -0.006 | 0 | 0 |
| 29 |  |  | 4 | 0 | 0 | 0 | -0.006 | 0.006 | 0 | 0 |
| 30 |  |  | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 31 | 1 | M7 | 1 | 0 | 0.414 | 0.005 | 0 | 0 | 0 | 0 |
| 32 |  |  | 2 | 0 | 0.37 | 0.005 | 2.067 | -2.067 | 0.208 | -0.208 |
| 33 |  |  | 3 | 0 | 0 | 0 | 2.371 | -2.371 | 0.228 | -0.228 |
| 34 |  |  | 4 | 0 | -0.37 | -0.005 | 2.067 | -2.067 | 0.208 | -0.208 |
| 35 |  |  | 5 | 0 | -0.414 | -0.005 | 0 | 0 | 0 | 0 |
| 36 | 1 | M8 | 1 | 0.018 | 0.359 | 0 | -0.033 | 0.033 | 0 | 0 |
| 37 |  |  | 2 | 0.011 | 0.127 | 0 | 1.883 | -1.883 | 0 | 0 |
| 38 |  |  | 3 | 0.004 | -0.105 | 0 | 1.971 | -1.971 | 0 | 0 |
| 39 |  |  | 4 | -0.003 | -0.338 | 0 | 0.23 | -0.23 | 0.002 | -0.002 |
| 40 |  |  | 5 | 0 | -0.024 | 0 | -0.011 | 0.011 | 0 | 0 |
| 41 | 1 | M9 | 1 | 0.018 | 0.359 | 0 | -0.033 | 0.033 | 0 | 0 |
| 42 |  |  | 2 | 0.011 | 0.127 | 0 | 1.883 | -1.883 | 0 | 0 |
| 43 |  |  | 3 | 0.004 | -0.105 | 0 | 1.971 | -1.971 | 0 | 0 |
| 44 |  |  | 4 | -0.003 | -0.338 | 0 | 0.23 | -0.23 | -0.002 | 0.002 |
| 45 |  |  | 5 | 0 | -0.024 | 0 | -0.011 | 0.011 | 0 | 0 |
| 46 | 2 | M1 | 1 | 0.007 | 0.202 | 0 | 0.055 | -0.055 | 0 | 0 |
| 47 |  |  | 2 | 0.002 | 0.05 | 0 | 1.05 | -1.05 | 0 | 0 |
| 48 |  |  | 3 | -0.002 | -0.102 | 0 | 0.847 | -0.847 | 0 | 0 |
| 49 |  |  | 4 | -0.007 | -0.255 | 0 | -0.556 | 0.556 | 0 | 0 |
| 50 |  |  | 5 | 0.001 | 0.045 | 0 | 0.023 | -0.023 | 0 | 0 |
| 51 | 2 | M2 | 1 | 0.007 | 0.202 | 0 | 0.055 | -0.055 | 0 | 0 |
| 52 |  |  | 2 | 0.002 | 0.05 | 0 | 1.05 | -1.05 | 0 | 0 |
| 53 |  |  | 3 | -0.002 | -0.102 | 0 | 0.847 | -0.847 | 0 | 0 |
| 54 |  |  | 4 | -0.007 | -0.255 | 0 | -0.556 | 0.556 | 0 | 0 |
| 55 |  |  | 5 | 0.001 | 0.045 | 0 | 0.023 | -0.023 | 0 | 0 |
| 56 | 2 | M5 | 1 | 0.493 | 0 | -0.024 | 0 | 0 | 0.423 | -0.423 |
| 57 |  |  | 2 | 0.493 | 0 | -0.024 | 0 | 0 | 0.106 | -0.106 |
| 58 |  |  | 3 | 0.493 | 0 | -0.024 | 0 | 0 | -0.211 | 0.211 |
| 59 |  |  | 4 | 0.493 | 0 | -0.024 | 0 | 0 | -0.529 | 0.529 |
| 60 |  |  | 5 | 0.493 | 0 | -0.024 | 0 | 0 | -0.846 | 0.846 |
| 61 | 2 | M6 | 1 | 0.493 | 0 | -0.024 | 0 | 0 | 0.423 | -0.423 |
| 62 |  |  | 2 | 0.493 | 0 | -0.024 | 0 | 0 | 0.106 | -0.106 |
| 63 |  |  | 3 | 0.493 | 0 | -0.024 | 0 | 0 | -0.211 | 0.211 |
| 64 |  |  | 4 | 0.493 | 0 | -0.024 | 0 | 0 | -0.529 | 0.529 |
| 65 |  |  | 5 | 0.493 | 0 | -0.024 | 0 | 0 | -0.846 | 0.846 |
| 66 | 2 | M5A | 1 | 0 | 0.007 | 0 | 0 | 0 | 0 | 0 |
| 67 |  |  | 2 | 0 | 0.007 | 0 | 0.174 | -0.174 | -0.004 | 0.004 |
| 68 |  |  | 3 | 0 | 0 | 0 | 0.196 | -0.196 | -0.004 | 0.004 |
| 69 |  |  | 4 | 0 | -0.007 | 0 | 0.174 | -0.174 | -0.004 | 0.004 |
| 70 |  |  | 5 | 0 | -0.007 | 0 | 0 | 0 | 0 | 0 |
| 71 | 2 | M6A | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 72 |  |  | 2 | 0 | 0 | 0 | -0.001 | 0.001 | 0 | 0 |
| 73 |  |  | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 74 |  |  | 4 | 0 | 0 | 0 | -0.001 | 0.001 | 0 | 0 |
| 75 |  |  | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 76 | 2 | M7 | 1 | 0 | 0.558 | 0.007 | 0 | 0 | 0 | 0 |
| 77 |  |  | 2 | 0 | 0.558 | 0.007 | 2.942 | -2.942 | 0.292 | -0.292 |
| 78 |  |  | 3 | 0 | 0 | 0 | 3.265 | -3.265 | 0.318 | -0.318 |
| 79 |  |  | 4 | 0 | -0.558 | -0.007 | 2.942 | -2.942 | 0.292 | -0.292 |
| 80 |  |  | 5 | 0 | -0.558 | -0.007 | 0 | 0 | 0 | 0 |


|  | LC | Member L.. | Sec | Axial [ksi] | y Shear [ksi] | z Shear [ksi] | y top Bend.. | y bot Bend... | z top Bend... | z bot Bend... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81 | 2 | M8 | 1 | 0.029 | 0.612 | 0 | -0.055 | 0.055 | -0.002 | 0.002 |
| 82 |  |  | 2 | 0.017 | 0.216 | 0 | 3.21 | -3.21 | 0 | 0 |
| 83 |  |  | 3 | 0.005 | -0.179 | 0 | 3.36 | -3.36 | 0.001 | -0.001 |
| 84 |  |  | 4 | -0.008 | -0.576 | 0 | 0.391 | -0.391 | 0.003 | -0.003 |
| 85 |  |  | 5 | -0.001 | -0.045 | 0 | -0.023 | 0.023 | 0.002 | -0.002 |
| 86 | 2 | M9 | 1 | 0.029 | 0.612 | 0 | -0.055 | 0.055 | 0.002 | -0.002 |
| 87 |  |  | 2 | 0.017 | 0.216 | 0 | 3.21 | -3.21 | 0 | 0 |
| 88 |  |  | 3 | 0.005 | -0.179 | 0 | 3.36 | -3.36 | -0.001 | 0.001 |
| 89 |  |  | 4 | -0.008 | -0.576 | 0 | 0.391 | -0.391 | -0.003 | 0.003 |
| 90 |  |  | 5 | -0.001 | -0.045 | 0 | -0.023 | 0.023 | -0.002 | 0.002 |
| 91 | 3 | M1 | 1 | 0.012 | 0.348 | 0 | 0.088 | -0.088 | 0 | 0 |
| 92 |  |  | 2 | 0.004 | 0.086 | 0 | 1.8 | -1.8 | 0 | 0 |
| 93 |  |  | 3 | -0.004 | -0.176 | 0 | 1.446 | -1.446 | 0 | 0 |
| 94 |  |  | 4 | -0.012 | -0.44 | 0 | -0.976 | 0.976 | 0 | 0 |
| 95 |  |  | 5 | 0.003 | 0.085 | 0 | 0.033 | -0.033 | 0 | 0 |
| 96 | 3 | M2 | 1 | 0.012 | 0.348 | 0 | 0.088 | -0.088 | 0 | 0 |
| 97 |  |  | 2 | 0.004 | 0.086 | 0 | 1.8 | -1.8 | 0 | 0 |
| 98 |  |  | 3 | -0.004 | -0.176 | 0 | 1.446 | -1.446 | 0 | 0 |
| 99 |  |  | 4 | -0.012 | -0.44 | 0 | -0.976 | 0.976 | 0 | 0 |
| 100 |  |  | 5 | 0.003 | 0.085 | 0 | 0.033 | -0.033 | 0 | 0 |
| 101 | 3 | M5 | 1 | 0.883 | 0 | -0.041 | 0 | 0 | 0.71 | -0.71 |
| 102 |  |  | 2 | 0.877 | 0 | -0.041 | 0 | 0 | 0.178 | -0.178 |
| 103 |  |  | 3 | 0.87 | 0 | -0.041 | 0 | 0 | -0.354 | 0.354 |
| 104 |  |  | 4 | 0.864 | 0 | -0.041 | 0 | 0 | -0.887 | 0.887 |
| 105 |  |  | 5 | 0.857 | 0 | -0.041 | 0 | 0 | -1.419 | 1.419 |
| 106 | 3 | M6 | 1 | 0.883 | 0 | -0.041 | 0 | 0 | 0.71 | -0.71 |
| 107 |  |  | 2 | 0.877 | 0 | -0.041 | 0 | 0 | 0.178 | -0.178 |
| 108 |  |  | 3 | 0.87 | 0 | -0.041 | 0 | 0 | -0.354 | 0.354 |
| 109 |  |  | 4 | 0.864 | 0 | -0.041 | 0 | 0 | -0.887 | 0.887 |
| 110 |  |  | 5 | 0.857 | 0 | -0.041 | 0 | 0 | -1.419 | 1.419 |
| 111 | 3 | M5A | 1 | 0 | 0.014 | 0 | 0 | 0 | 0 | 0 |
| 112 |  |  | 2 | 0 | 0.012 | 0 | 0.312 | -0.312 | -0.007 | 0.007 |
| 113 |  |  | 3 | 0 | 0 | 0 | 0.361 | -0.361 | -0.007 | 0.007 |
| 114 |  |  | 4 | 0 | -0.012 | 0 | 0.312 | -0.312 | -0.007 | 0.007 |
| 115 |  |  | 5 | 0 | -0.014 | 0 | 0 | 0 | 0 | 0 |
| 116 | 3 | M6A | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 117 |  |  | 2 | 0 | 0 | 0 | -0.007 | 0.007 | 0 | 0 |
| 118 |  |  | 3 | 0 | 0 | 0 | 0.006 | -0.006 | 0 | 0 |
| 119 |  |  | 4 | 0 | 0 | 0 | -0.007 | 0.007 | 0 | 0 |
| 120 |  |  | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 121 | 3 | M7 | 1 | 0 | 0.973 | 0.012 | 0 | 0 | 0 | 0 |
| 122 |  |  | 2 | 0 | 0.929 | 0.012 | 5.009 | -5.009 | 0.5 | -0.5 |
| 123 |  |  | 3 | 0 | 0 | 0 | 5.637 | -5.637 | 0.546 | -0.546 |
| 124 |  |  | 4 | 0 | -0.929 | -0.012 | 5.009 | -5.009 | 0.5 | -0.5 |
| 125 |  |  | 5 | 0 | -0.973 | -0.012 | 0 | 0 | 0 | 0 |
| 126 | 3 | M8 | 1 | 0.047 | 0.97 | 0 | -0.088 | 0.088 | -0.003 | 0.003 |
| 127 |  |  | 2 | 0.028 | 0.344 | 0 | 5.093 | -5.093 | 0 | 0 |
| 128 |  |  | 3 | 0.008 | -0.283 | 0 | 5.331 | -5.331 | 0.002 | -0.002 |
| 129 |  |  | 4 | -0.011 | -0.914 | 0 | 0.621 | -0.621 | 0.005 | -0.005 |
| 130 |  |  | 5 | -0.002 | -0.069 | 0 | -0.033 | 0.033 | 0.003 | -0.003 |
| 131 | 3 | M9 | 1 | 0.047 | 0.97 | 0 | -0.088 | 0.088 | 0.003 | -0.003 |
| 132 |  |  | 2 | 0.028 | 0.344 | 0 | 5.093 | -5.093 | 0 | 0 |
| 133 |  |  | 3 | 0.008 | -0.283 | 0 | 5.331 | -5.331 | -0.002 | 0.002 |
| 134 |  |  | 4 | -0.011 | -0.914 | 0 | 0.621 | -0.621 | -0.005 | 0.005 |
| 135 |  |  | 5 | -0.002 | -0.069 | 0 | -0.033 | 0.033 | -0.003 | 0.003 |

## Asd360

| LC |  | Member | Shape | UC Max | Loc [ft] | Shear... Loc [ft] |  | Dir | Pnc/o... Pnt/om... Mnyy/o... Mnzz/o.. |  |  |  | Cb | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | W4X13 | 0.023 | 4.087 | 0.010 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.438 | 1.26 | H1-1b |
| 2 | 1 | M2 | W4X13 | 0.023 | 4.087 | 0.010 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.438 | 1.26 | H1-1b |
| 3 | 1 | M5 | PIPE_... | 0.023 | 7.5 | 0.001 | 7.5 |  | 72.95 | 102.695 | 10.155 | 10.155 | 1 | H1-1b |


|  | LC | Member | Shape | UC Max | Loc [ft] | Shear.. | Loc [ft] | Dir | Pnc/o. | Pnt/om | Mnyy/o | Mnzz/o | Cb | Eqn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 1 | M6 | PIPE | 0.023 | 7.5 | 0.001 | 7.5 |  | 72.95 | 102.695 | 10.155 | 10.155 | 1 | H1-1b |
| 5 | 1 | M7 | W6X25 | 0.086 | 7.2 | 0.024 | 14.4 | y | 86.09 | 219.76 | 21.357 | 40.868 | 1.066 | H1-1b |
| 6 | 1 | M8 | W4X13 | 0.063 | 4.726 | 0.022 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.669 | 1.375 | H1-1b |
| 7 | 1 | M9 | W4X13 | 0.063 | 4.726 | 0.022 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.669 | 1.375 | H1-1b |
| 8 | 2 | M1 | W4X13 | 0.033 | 4.087 | 0.014 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.543 | 1.268 | H1-1b |
| 9 | 2 | M2 | W4X13 | 0.033 | 4.087 | 0.014 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.543 | 1.268 | H1-1b |
| 10 | 2 | M5 | PIPE | 0.032 | 7.5 | 0.001 | 7.5 |  | 72.95 | 102.695 | 10.155 | 10.155 | 1 | H1-1b |
| 11 | 2 | M6 | PIPE | 0.032 | 7.5 | 0.001 | 7.5 |  | 72.95 | 102.695 | 10.155 | 10.155 | 1 | H1-1b |
| 12 | 2 | M7 | W6X25 | 0.120 | 10.35 | 0.035 | 14.4 | y | 86.09 | 219.76 | 21.357 | 40.259 | 1.05 | H1-1b |
| 13 | 2 | M8 | W4X13 | 0.107 | 4.726 | 0.036 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.669 | 1.375 | H1-1b |
| 14 | 2 | M9 | W4X13 | 0.107 | 4.726 | 0.036 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.669 | 1.375 | H1-1b |
| 15 | 3 | M1 | W4X13 | 0.056 | 4.087 | 0.025 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.499 | 1.265 | H1-1b |
| 16 | 3 | M2 | W4X13 | 0.056 | 4.087 | 0.025 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.499 | 1.265 | H1-1b |
| 17 | 3 | M5 | PIPE | 0.055 | 7.5 | 0.002 | 7.5 |  | 72.95 | 102.695 | 10.155 | 10.155 | 1 | H1-1b |
| 18 | 3 | M6 | PIPE | 0.055 | 7.5 | 0.002 | 7.5 |  | 72.95 | 102.695 | 10.155 | 10.155 | 1 | H1-1b |
| 19 | 3 | M7 | W6X25 | 0.206 | 7.2 | 0.058 | 14.4 | y | 86.09 | 219.76 | 21.357 | 40.513 | 1.056 | H1-1b |
| 20 | 3 | M8 | W4X13 | 0.170 | 4.726 | 0.058 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.669 | 1.375 | H1-1b |
| 21 | 3 | M9 | W4X13 | 0.170 | 4.726 | 0.058 | 9.835 | y | 26.796 | 114.671 | 7.285 | 15.669 | 1.375 | H1-1b |

## Warning Log

## Member Section Deflections Strength

|  | LC | Member Label | Sec | $x$ [in] | $y[i n]$ | z [in] | $x$ Rotate [rad] | (n) L/y' Ratio | (n) L/z' Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | M1 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 2 |  |  | 2 | 0 | -0.019 | 0 | 0 | 7345 | NC |
| 3 |  |  | 3 | 0 | -0.019 | 0 | 0 | 6985 | NC |
| 4 |  |  | 4 | 0 | -0.005 | 0 | 0 | NC | NC |
| 5 |  |  | 5 | 0 | 0.004 | 0 | 0 | NC | NC |
| 6 | 1 | M2 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 7 |  |  | 2 | 0 | -0.019 | 0 | 0 | 7345 | NC |
| 8 |  |  | 3 | 0 | -0.019 | 0 | 0 | 6985 | NC |
| 9 |  |  | 4 | 0 | -0.005 | 0 | 0 | NC | NC |
| 10 |  |  | 5 | 0 | 0.004 | 0 | 0 | NC | NC |
| 11 | 1 | M5 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 12 |  |  | 2 | 0 | 0 | 0.001 | 0 | NC | NC |
| 13 |  |  | 3 | 0 | 0 | 0.003 | 0 | NC | NC |
| 14 |  |  | 4 | -0.001 | 0 | 0.004 | 0 | NC | NC |
| 15 |  |  | 5 | -0.001 | 0 | 0 | 0 | NC | NC |
| 16 | 1 | M6 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 17 |  |  | 2 | 0 | 0 | 0.001 | 0 | NC | NC |
| 18 |  |  | 3 | 0 | 0 | 0.003 | 0 | NC | NC |
| 19 |  |  | 4 | -0.001 | 0 | 0.004 | 0 | NC | NC |
| 20 |  |  | 5 | -0.001 | 0 | 0 | 0 | NC | NC |
| 21 | 1 | M5A | 1 | 0 | 0.004 | 0 | -1.615e-04 | NC | NC |
| 22 |  |  | 2 | 0 | -0.059 | 0.006 | -7.106e-04 | 2751 | NC |
| 23 |  |  | 3 | 0 | -0.084 | 0.008 | -7.717e-04 | 1976 | NC |
| 24 |  |  | 4 | 0 | -0.059 | 0.006 | -7.106e-04 | 2751 | NC |
| 25 |  |  | 5 | 0 | 0.004 | 0 | -1.615e-04 | NC | NC |
| 26 | 1 | M6A | 1 | 0 | 0 | 0 | $6.545 \mathrm{e}-04$ | NC | NC |
| 27 |  |  | 2 | 0 | 0 | 0 | $2.303 \mathrm{e}-03$ | NC | NC |
| 28 |  |  | 3 | 0 | 0 | 0 | 2.486e-03 | NC | NC |
| 29 |  |  | 4 | 0 | 0 | 0 | $2.303 \mathrm{e}-03$ | NC | NC |
| 30 |  |  | 5 | 0 | 0 | 0 | $6.545 \mathrm{e}-04$ | NC | NC |
| 31 | 1 | M7 | 1 | 0 | -0.001 | 0 | $2.773 \mathrm{e}-04$ | NC | NC |
| 32 |  |  | 2 | 0 | -0.079 | -0.008 | 7.961e-04 | 2215 | NC |
| 33 |  |  | 3 | 0 | -0.109 | -0.011 | $8.538 \mathrm{e}-04$ | 1602 | NC |
| 34 |  |  | 4 | 0 | -0.079 | -0.008 | $7.961 \mathrm{e}-04$ | 2215 | NC |
| 35 |  |  | 5 | 0 | -0.001 | 0 | $2.773 \mathrm{e}-04$ | NC | NC |
| 36 | 1 | M8 | 1 | 0 | 0 | 0 | -9.447e-06 | NC | NC |
| 37 |  |  | 2 | 0 | -0.081 | 0 | -3.827e-04 | 2277 | NC |

Company
BCQ
2/4/2022
Designer

## Member Section Deflections Strength (Continued)

|  | LC | Member Label | Sec | $x$ [in] | y [in] | z [in] | x Rotate [rad] | (n) L/y' Ratio | (n) L/z' Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 38 |  |  | 3 | 0 | -0.113 | 0 | -7.559e-04 | 1823 | NC |
| 39 |  |  | 4 | 0 | -0.094 | 0 | -1.129e-03 | 3214 | NC |
| 40 |  |  | 5 | 0 | -0.065 | 0 | -1.007e-03 | 2278 | NC |
| 41 | 1 | M9 | 1 | 0 | 0 | 0 | $9.447 \mathrm{e}-06$ | NC | NC |
| 42 |  |  | 2 | 0 | -0.081 | 0 | $3.827 \mathrm{e}-04$ | 2277 | NC |
| 43 |  |  | 3 | 0 | -0.113 | 0 | $7.559 \mathrm{e}-04$ | 1823 | NC |
| 44 |  |  | 4 | 0 | -0.094 | 0 | $1.129 \mathrm{e}-03$ | 3214 | NC |
| 45 |  |  | 5 | 0 | -0.065 | 0 | 1.007e-03 | 2278 | NC |
| 46 | 2 | M1 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 47 |  |  | 2 | 0 | -0.027 | 0 | 0 | 5170 | NC |
| 48 |  |  | 3 | 0 | -0.027 | 0 | 0 | 4862 | NC |
| 49 |  |  | 4 | 0 | -0.006 | 0 | 0 | NC | NC |
| 50 |  |  | 5 | 0 | 0.006 | 0 | 0 | NC | NC |
| 51 | 2 | M2 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 52 |  |  | 2 | 0 | -0.027 | 0 | 0 | 5170 | NC |
| 53 |  |  | 3 | 0 | -0.027 | 0 | 0 | 4862 | NC |
| 54 |  |  | 4 | 0 | -0.006 | 0 | 0 | NC | NC |
| 55 |  |  | 5 | 0 | 0.006 | 0 | 0 | NC | NC |
| 56 | 2 | M5 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 57 |  |  | 2 | 0 | 0 | 0.002 | 0 | NC | NC |
| 58 |  |  | 3 | 0 | 0 | 0.005 | 0 | NC | NC |
| 59 |  |  | 4 | -0.001 | 0 | 0.005 | $4.029 \mathrm{e}-08$ | NC | NC |
| 60 |  |  | 5 | -0.002 | 0 | 0 | $5.372 \mathrm{e}-08$ | NC | NC |
| 61 | 2 | M6 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 62 |  |  | 2 | 0 | 0 | 0.002 | 0 | NC | NC |
| 63 |  |  | 3 | 0 | 0 | 0.005 | 0 | NC | NC |
| 64 |  |  | 4 | -0.001 | 0 | 0.005 | -4.029e-08 | NC | NC |
| 65 |  |  | 5 | -0.002 | 0 | 0 | -5.372e-08 | NC | NC |
| 66 | 2 | M5A | 1 | 0 | 0.006 | 0 | -2.673e-04 | NC | NC |
| 67 |  |  | 2 | 0 | -0.071 | 0.007 | -1.41e-03 | 2242 | NC |
| 68 |  |  | 3 | 0 | -0.101 | 0.01 | -1.537e-03 | 1617 | NC |
| 69 |  |  | 4 | 0 | -0.071 | 0.007 | -1.41e-03 | 2242 | NC |
| 70 |  |  | 5 | 0 | 0.006 | 0 | -2.673e-04 | NC | NC |
| 71 | 2 | M6A | 1 | 0 | 0 | 0 | $9.218 \mathrm{e}-04$ | NC | NC |
| 72 |  |  | 2 | 0 | 0 | 0 | $3.708 \mathrm{e}-03$ | NC | NC |
| 73 |  |  | 3 | 0 | 0 | 0 | $4.018 \mathrm{e}-03$ | NC | NC |
| 74 |  |  | 4 | 0 | 0 | 0 | $3.708 \mathrm{e}-03$ | NC | NC |
| 75 |  |  | 5 | 0 | 0 | 0 | $9.218 \mathrm{e}-04$ | NC | NC |
| 76 | 2 | M7 | 1 | 0 | -0.002 | 0 | 4.1e-04 | NC | NC |
| 77 |  |  | 2 | 0 | -0.111 | -0.011 | $1.55 \mathrm{e}-03$ | 1582 | NC |
| 78 |  |  | 3 | 0 | -0.153 | -0.015 | $1.676 \mathrm{e}-03$ | 1147 | NC |
| 79 |  |  | 4 | 0 | -0.111 | -0.011 | $1.55 \mathrm{e}-03$ | 1582 | NC |
| 80 |  |  | 5 | 0 | -0.002 | 0 | 4.1e-04 | NC | NC |
| 81 | 2 | M8 | 1 | 0 | 0 | 0 | -4.32e-06 | NC | NC |
| 82 |  |  | 2 | 0 | -0.13 | 0 | -5.277e-04 | 1335 | NC |
| 83 |  |  | 3 | 0 | -0.176 | 0 | -1.051e-03 | 1069 | NC |
| 84 |  |  | 4 | 0 | -0.136 | 0 | -1.574e-03 | 1885 | NC |
| 85 |  |  | 5 | 0 | -0.078 | 0 | -1.23e-03 | 1898 | NC |
| 86 | 2 | M9 | 1 | 0 | 0 | 0 | 4.32e-06 | NC | NC |
| 87 |  |  | 2 | 0 | -0.13 | 0 | $5.277 \mathrm{e}-04$ | 1335 | NC |
| 88 |  |  | 3 | 0 | -0.176 | 0 | $1.051 \mathrm{e}-03$ | 1069 | NC |
| 89 |  |  | 4 | 0 | -0.136 | 0 | $1.574 \mathrm{e}-03$ | 1885 | NC |
| 90 |  |  | 5 | 0 | -0.078 | 0 | 1.23e-03 | 1898 | NC |
| 91 | 3 | M1 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 92 |  |  | 2 | 0 | -0.046 | 0 | 0 | 3034 | NC |
| 93 |  |  | 3 | 0 | -0.046 | 0 | 0 | 2866 | NC |
| 94 |  |  | 4 | 0 | -0.011 | 0 | 0 | 7975 | NC |
| 95 |  |  | 5 | 0 | 0.01 | 0 | 0 | NC | NC |
| 96 | 3 | M2 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 97 |  |  | 2 | 0 | -0.046 | 0 | 0 | 3034 | NC |
| 98 |  |  | 3 | 0 | -0.046 | 0 | 0 | 2866 | NC |
| 99 |  |  | 4 | 0 | -0.011 | 0 | 0 | 7975 | NC |

$\qquad$

## Member Section Deflections Strength (Continued)

|  | LC | Member Label | Sec | $x$ [in] | $y[i n]$ | z [in] | $x$ Rotate [rad] | (n) L/y' Ratio | (n) L/z' Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 |  |  | 5 | 0 | 0.01 | 0 | 0 | NC | NC |
| 101 | 3 | M5 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 102 |  |  | 2 | 0 | 0 | 0.003 | 0 | NC | NC |
| 103 |  |  | 3 | -0.002 | 0 | 0.008 | $4.128 \mathrm{e}-08$ | NC | NC |
| 104 |  |  | 4 | -0.003 | 0 | 0.009 | $6.193 \mathrm{e}-08$ | NC | NC |
| 105 |  |  | 5 | -0.003 | 0 | 0 | $8.257 \mathrm{e}-08$ | NC | NC |
| 106 | 3 | M6 | 1 | 0 | 0 | 0 | 0 | NC | NC |
| 107 |  |  | 2 | 0 | 0 | 0.003 | 0 | NC | NC |
| 108 |  |  | 3 | -0.002 | 0 | 0.008 | -4.128e-08 | NC | NC |
| 109 |  |  | 4 | -0.003 | 0 | 0.009 | -6.193e-08 | NC | NC |
| 110 |  |  | 5 | -0.003 | 0 | 0 | -8.257e-08 | NC | NC |
| 111 | 3 | M5A | 1 | 0 | 0.01 | 0 | -4.289e-04 | NC | NC |
| 112 |  |  | 2 | 0 | -0.13 | 0.013 | -2.121e-03 | 1235 | NC |
| 113 |  |  | 3 | 0 | -0.184 | 0.018 | -2.309e-03 | 889 | 8867 |
| 114 |  |  | 4 | 0 | -0.13 | 0.013 | -2.121e-03 | 1235 | NC |
| 115 |  |  | 5 | 0 | 0.01 | 0 | -4.289e-04 | NC | NC |
| 116 | 3 | M6A | 1 | 0 | 0 | 0 | $1.576 \mathrm{e}-03$ | NC | NC |
| 117 |  |  | 2 | 0 | 0 | 0 | $6.011 \mathrm{e}-03$ | NC | NC |
| 118 |  |  | 3 | 0 | 0 | 0 | $6.504 \mathrm{e}-03$ | NC | NC |
| 119 |  |  | 4 | 0 | 0 | 0 | $6.011 \mathrm{e}-03$ | NC | NC |
| 120 |  |  | 5 | 0 | 0 | 0 | 1.576e-03 | NC | NC |
| 121 | 3 | M7 | 1 | 0 | -0.003 | 0 | $6.874 \mathrm{e}-04$ | NC | NC |
| 122 |  |  | 2 | 0 | -0.191 | -0.019 | $2.346 \mathrm{e}-03$ | 923 | 9167 |
| 123 |  |  | 3 | 0 | -0.262 | -0.026 | $2.53 \mathrm{e}-03$ | 668 | 6626 |
| 124 |  |  | 4 | 0 | -0.191 | -0.019 | $2.346 \mathrm{e}-03$ | 923 | 9167 |
| 125 |  |  | 5 | 0 | -0.003 | 0 | $6.874 \mathrm{e}-04$ | NC | NC |
| 126 | 3 | M8 | 1 | 0 | 0 | 0 | -1.377e-05 | NC | NC |
| 127 |  |  | 2 | 0 | -0.21 | 0 | -9.104e-04 | 842 | NC |
| 128 |  |  | 3 | 0 | -0.289 | 0 | -1.807e-03 | 674 | NC |
| 129 |  |  | 4 | 0 | -0.23 | 0 | $-2.704 \mathrm{e}-03$ | 1188 | NC |
| 130 |  |  | 5 | 0 | -0.142 | 0 | -2.238e-03 | 1035 | NC |
| 131 | 3 | M9 | 1 | 0 | 0 | 0 | $1.377 \mathrm{e}-05$ | NC | NC |
| 132 |  |  | 2 | 0 | -0.21 | 0 | $9.104 \mathrm{e}-04$ | 842 | NC |
| 133 |  |  | 3 | 0 | -0.289 | 0 | $1.807 \mathrm{e}-03$ | 674 | NC |
| 134 |  |  | 4 | 0 | -0.23 | 0 | $2.704 \mathrm{e}-03$ | 1188 | NC |
| 135 |  |  | 5 | 0 | -0.142 | 0 | $2.238 \mathrm{e}-03$ | 1035 | NC |




All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 563 @ 12' 9 1/2" | 910 (1.75") | Passed (62\%) | 1.00 | 1.0 D + 1.0 L (All Spans) |  |
| Shear (lbs) | 563 @ 12' 9 1/2" | 1860 | Passed (30\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Moment (Ft-lbs) | 1747 @ 6' 7" | 3740 | Passed (47\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Live Load Defl. (in) | 0.074 @ 6' 7" | 0.310 | Passed (L/999+) | -- | 1.0 D + 1.0 L (All Spans) |  |
| Total Load Defl. (in) | 0.126 @ 6' 7" | 0.621 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 65 | 40 | Passed | -- | -- |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of $23 / 32$ " Weyerhaeuser Edge ${ }^{T M}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 246 | 351 | 597 | Blocking |
| 2-Hanger on 14" HF beam | $3.50^{\prime \prime}$ | Hanger $^{1}$ | $1.75^{\prime \prime} /-^{2}$ | 243 | 347 | 590 | See note $^{1}$ |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.
- 2 Required Bearing Length / Required Bearing Length with Web Stiffeners

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} \mathrm{g}^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $12^{\prime} 10 \mathrm{o}$ o/c |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.
-Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| 2 - Face Mount Hanger | IUS1.81/14 | 2.00 | N/A | 12-10dx1.5 | 2-Strong-Grip |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Load | Location | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $13^{\prime} 1^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator


Job Notes


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $548 @ 11^{\prime} 61 / 2^{\prime \prime}$ | $1375\left(3.500^{\prime \prime}\right)$ | Passed (40\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $506 @ 1 / 2^{\prime \prime}$ | 1860 | Passed (27\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $1456 @ 5^{\prime} 101 / 2^{\prime \prime}$ | 3740 | Passed (39\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.054 @ 5^{\prime} 101 / 2^{\prime \prime}$ | 0.283 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Building Use : Joist |  |  |  |  |  |
| Building Codential $:$ IBC 2018 |  |  |  |  |  |
| Total Load Defl. (in) | $0.091 @ 5^{\prime} 101 / 2^{\prime \prime}$ | 0.567 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 69 | 40 | Passed | -- | -- |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 219 | 313 | 532 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 226 | 322 | 548 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $5^{\prime} 2 " \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $11^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $11^{\prime} 11^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
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| jaj@bcq-se.com |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $1027 @ 17^{\prime} 101 / 2^{\prime \prime}$ | $1080\left(1.75^{\prime \prime}\right)$ | Passed (95\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $1027 @ 17^{\prime} 101 / 2^{\prime \prime}$ | 1705 | Passed (60\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $4492 @ 9^{\prime} 11 / 2^{\prime \prime}$ | 6180 | Passed (73\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.395 @ 9^{\prime} 11 / 2^{\prime \prime}$ | 0.438 | Passed (L/532) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Building Use : Residential |  |  |  |  |  |
| Building Code : IBC 2018 |  |  |  |  |  |
| Total Load Defl. (in) | $0.579 @ 9^{\prime} 11 / 2^{\prime \prime}$ | 0.875 | Passed (L/363) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 51 | 40 | Passed | -- | -- |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. $8^{\prime}$ o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Stud wall - HF | 5.50" | 5.50" | 1.75" | 341 | 730 | 1071 | Blocking |
| 2 - Hanger on $117 / 8^{\prime \prime} \mathrm{HF}$ beam | 5.50" | Hanger ${ }^{1}$ | 1.75" / - 2 | 344 | 737 | 1081 | See note ${ }^{1}$ |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.
- 2 Required Bearing Length / Required Bearing Length with Web Stiffeners

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} 3^{\prime \prime} \circ / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $17^{\prime} 11^{\prime \prime} \circ / \mathrm{c}$ |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.
-Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| 2 - Face Mount Hanger | U3516/20 | $2.00 "$ | N/A | $16-10 \mathrm{~d} \times 1.5$ | $6-10 \mathrm{~d} \times 1.5$ | Web Stiffeners |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Load | Location | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $18^{\prime} 4^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator


Job Notes


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 733 @ 4 1/2" | 1375 (3.50") | Passed (53\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Shear (lbs) | 680 @ $51 / 2^{\prime \prime}$ | 1560 | Passed (44\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Moment (Ft-lbs) | 2025 @ 6' 3" | 3160 | Passed (64\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Live Load Defl. (in) | 0.127 @ 6' 3" | 0.294 | Passed (L/999+) | -- | 1.0 D + 1.0 L (All Spans) |  |
| Total Load Defl. (in) | 0.186 @ 6' 3" | 0.587 | Passed (L/757) | -- | 1.0 D + 1.0 L (All Spans) |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 66 | 40 | Passed | -- | -- |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
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- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 233 | 500 | 733 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 233 | 500 | 733 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} 6 \mathrm{o} \circ \mathrm{c}$ |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $12^{\prime} 6^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
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## Upper Floor, B6

$\mathbf{2}$ piece(s) $\mathbf{2 \times 8} \mathbf{~ H F}$ No. 2


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $710 @ 4 "$ | $6683(5.50 ")$ | Passed (11\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $573 @ 11^{\prime} 3 / 4 "$ | 2501 | Passed (23\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | 1724 @ 5' 6" | 2569 | Passed (67\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.155 @ 5^{\prime} 6 "$ | 0.258 | Passed (L/798) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | $0.268 @ 5^{\prime} 6^{\prime \prime}$ | 0.517 | Passed (L/463) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1-Stud wall - HF | 5.50" | 5.50 " | $1.50{ }^{\prime \prime}$ | 298 | 220 | 330 | 848 | Blocking |
| 2 - Stud wall - HF | 5.50" | 5.50" | 1.50" | 298 | 220 | 330 | 848 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $11^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $11^{\prime} \mathrm{o} / \mathrm{c}$ |  |

$\bullet$ Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
| Bykonen Carter Quinn |  |
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| jaj@bcq-se.com |  |

1 piece(s) 3 1/2" $\times 11$ 7/8" $1.55 E$ TimberStrand $®$ LSL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 2882 @ 4" | 7796 (5.50") | Passed (37\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | 1598 @ 1' 5 3/8" | 9878 | Passed (16\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | 3772 @ 3' 3" | 18346 | Passed (21\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.025 @ 3' 3" | 0.146 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.044 @ 3' 3" | 0.292 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1 - Stud wall - HF | 5.50" | 5.50 " | 2.03" | 1260 | 775 | 1388 | 3423 | Blocking |
| 2 - Stud wall - HF | 5.50" | 5.50" | 2.03" | 1260 | 775 | 1388 | 3423 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 6 "$ o/c |  |
| Bottom Edge (Lu) | $6^{\prime} 6 "$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ (0.90) \end{gathered}$ | Floor Live (1.00) | $\begin{aligned} & \text { Snow } \\ & \text { (1.15) } \end{aligned}$ | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to 6' 6" | N/A | 13.0 | -- | -- |  |
| 1 - Uniform (PSF) | 0 to 6' 6" (Front) | 5' $111 / 2^{\prime \prime}$ | 28.0 | 40.0 | - | Deck Load |
| 2 - Uniform (PLF) | 0 to 6' 6" (Front) | N/A | 181.5 | - | 362.5 | Linked from: J2, Support 2 |
| 3 - Uniform (PLF) | 0 to 6' 6" (Front) | N/A | 26.5 | - | 64.5 | Linked from: J4, Support 2 |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator
ForteWEB Software Operator
Job Notes


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 5014 @ 4" | 11694 (5.50") | Passed (43\%) | -- | 1.0 D + 1.0 S (All Spans) |
| Shear (lbs) | 3830 @ 1'91/2" | 18676 | Passed (21\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Moment (Ft-lbs) | 17378 @ 7' 7" | 60297 | Passed (29\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.122 @ 7' 7" | 0.290 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.188 @ 7' 7" | 0.725 | Passed (L/923) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/600) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | 5.50" | 5.50" | 2.36 " | 1776 | 3238 | 5014 | Blocking |
| 2 - Stud wall - HF | 5.50" | 5.50" | 2.36 " | 1776 | 3238 | 5014 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $15^{\prime} 2$ " o/c |  |
| Bottom Edge (Lu) | $15^{\prime} 2$ " o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ (0.90) \end{gathered}$ | $\begin{aligned} & \text { Snow } \\ & (1.15) \end{aligned}$ | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to 15' ${ }^{\prime \prime}$ | N/A | 26.3 | -- |  |
| 1 - Uniform (PLF) | 0 to 15' 2" (Front) | N/A | 181.5 | 362.5 | Linked from: J2, Support 2 |
| 2 - Uniform (PLF) | 0 to 15' 2" (Front) | N/A | 26.5 | 64.5 | Linked from: J4, Support 2 |

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| ForteWEB Software Operator | Job Notes |
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1 piece(s) 3 1/2" x 14" $1.55 E$ TimberStrand ${ }^{\text {® }}$ LSL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $627 @ 2 "$ | 4961 (3.50") | Passed (13\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $473 @ 1^{\prime} 51 / 2^{\prime \prime}$ | 10127 | Passed (5\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $1752 @ 5^{\prime} 11^{\prime \prime}$ | 21840 | Passed (8\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.020 @ 5^{\prime} 11^{\prime \prime}$ | 0.287 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.039 @ 5^{\prime} 11^{\prime \prime}$ | 0.575 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Available | Required | Dead | Floor Live | Total | Accessories |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 312 | 316 | 628 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 320 | 324 | 644 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $12^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 15.3 | -- |  |
| 1 - Uniform (PSF) | 0 to $12^{\prime}$ (Front) | $1^{\prime} 4 \prime \prime$ | 28.0 | 40.0 | Floor Load |

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| (206) 264-7784 |  |
| jaj@bcq-se.com |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :--- | :--- |
| Member Reaction (lbs) | $9607 @ 2 "$ | $11340\left(3.50{ }^{\prime \prime}\right)$ | Passed (85\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $9349 @ 31 / 2^{\prime \prime}$ | 83570 | Passed (11\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $50273 @ 10^{\prime} 35 / 16^{\prime \prime}$ | 82296 | Passed (61\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.236 @ 12^{\prime} 11 / 16^{\prime \prime}$ | 0.613 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.433 @ 12^{\prime} 11 / 4^{\prime \prime}$ | 1.225 | Passed (L/679) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Applicable calculations are based on ANSI/AISC 360-16.
- A lateral-torsional buckling factor $(\mathrm{Cb})$ of 1.0 has been assumed.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | 4302 | 5305 | 9607 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | 3284 | 3865 | 7149 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :--- | :--- |
| Top Edge (Lu) | End Bearing Points |  |
| Bottom Edge (Lu) | End Bearing Points |  |


| Vertical Loads | Location (Side) | Tributary Width | Dead <br> (0.90) | Floor Live <br> (1.00) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0-Self Weight (PLF) | 0 to $25^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 43.0 | -- |  |
| 1 - Uniform (PLF) | 0 to $10^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 164.3 | 234.8 | Linked from: J2, <br> Support 1 |
| 2- Uniform (PLF) | 0 to $25^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 182.3 | 260.3 | Linked from: J1, <br> Support 2 |
| 3 - Point (lb) | $10^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 312 | 316 | Linked from: B9, <br> Support 1 |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $16583 @ 4 "$ | $17820(5.50 ")$ | Passed (93\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $16094 @ 51 / 2^{\prime \prime}$ | 83570 | Passed (19\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $96958 @ 8^{\prime} 6^{\prime \prime}$ | 110273 | Passed (88\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.299 @ 10^{\prime} 1 / 2^{\prime \prime}$ | 0.496 | Passed (L/796) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.507 @ 10^{\prime} 5 / 16^{\prime \prime}$ | 0.992 | Passed (L/469) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Applicable calculations are based on ANSI/AISC 360-16.
- A lateral-torsional buckling factor $(\mathrm{Cb})$ of 1.0 has been assumed.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1-Stud wall - HF | $5.50 "$ | $5.50 "$ | $5.50^{\prime \prime}$ | 6731 | 9851 | 728 | 17310 | Blocking |
| 2 - Stud wall - HF | $5.50 "$ | $5.50 "$ | $5.50 "$ | 5972 | 8915 | 728 | 15615 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :--- | :--- |
| Top Edge (Lu) | End Bearing Points |  |
| Bottom Edge (Lu) | End Bearing Points |  |


| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

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Upper Floor, B12
$\mathbf{2}$ piece(s) $\mathbf{2 \times 8} \mathbf{~ H F}$ No. 2


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 388 @ 4" | 6683 (5.50") | Passed (6\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | 250 @ 1' 3/4" | 2501 | Passed (10\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | 459 @ 3' | 2569 | Passed (18\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.011 @ 3' | 0.133 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.019 @ 3' | 0.267 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1-Stud wall - HF | 5.50" | 5.50 " | 1.50 " | 163 | 120 | 180 | 463 | Blocking |
| 2 - Stud wall - HF | 5.50" | 5.50" | 1.50" | 163 | 120 | 180 | 463 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $6^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> (0.90) | Floor Live <br> (1.00) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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## Upper Floor, B13 Corner Cantilever Rim Header

## 1 piece(s) 3 1/2" $\times 11$ 7/8" $1.55 E$ TimberStrand $®$ LSL



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $2087 @ 6^{\prime} 41 / 2^{\prime \prime}$ | $4253\left(3.00^{\prime \prime}\right)$ | Passed (49\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $1088 @ 77^{\prime} 57 / 8^{\prime \prime}$ | 8590 | Passed (13\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $-2637 @ 6^{\prime} 41 / 2^{\prime \prime}$ | 15953 | Passed (17\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.042 @ 9^{\prime} 6^{\prime \prime}$ | 0.200 | Passed (2L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.062 @ 9 ' 6 "$ | 0.313 | Passed (2L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Overhang deflection criteria: LL (2L/0.2") and TL (2L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- -380 lbs uplift at support located at $11 / 2^{\prime \prime}$. Strapping or other restraint may be required.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | 3.00" | 3.00" | 1.50" | -99 | -281 | -380 | Blocking |
| 2 - Stud wall - HF | 3.00" | 3.00 " | 1.50" | 726 | 1361 | 2087 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $9^{\prime} 6 " \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $9^{\prime} 6 \mathrm{o} ~ \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $9^{\prime} 6^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.0 | -- |  |
| 1 - Uniform (PSF) | $6^{\prime} 6^{\prime \prime}$ to $9^{\prime} 6^{\prime \prime}$ (Front) | $6^{\prime}$ | 28.0 | 60.0 | Deck |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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Upper Floor, Canopy Joist
1 piece(s) $2 \times 8$ HF No. 2 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 522 @ 4' 1 3/4" | 2126 (3.50") | Passed (25\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | 235 @ 4' 10 3/4" | 1251 | Passed (19\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | -515@ 4' 1 3/4" | 1477 | Passed (35\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.097 @ 0 | 0.207 | Passed (2L/999+) | -- | 1.0 D + 1.0 S (All Spans) |
| Total Load Defl. (in) | 0.132 @ 0 | 0.415 | Passed (2L/752) | -- | 1.0 D + 1.0 S (All Spans) |
| TJ-Pro ${ }^{\text {TM }}$ Rating | N/A | N/A | N/A | -- | N/A |

System : Floor Member Type : Joist Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240)
- Overhang deflection criteria: LL (2L/480) and TL (2L/240).
- Left cantilever length exceeds $1 / 3$ member length or $1 / 2$ back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 205 | 181 | 241 | 627 | Blocking |
| 2- Beam - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 46 | 186 | -81 | $232 /-81$ | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :---: | :---: | :---: |
| Top Edge (Lu) | 8'7" o/c |  |
| Bottom Edge (Lu) | 8' 7" o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $4^{\prime}$ | $16^{\prime \prime}$ | 15.0 | - | 30.0 | Default Load |
| 2 - Uniform (PSF) | $4^{\prime}$ to $8^{\prime} 7^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | - | Deck |

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Job Notes


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Wall <br> Member Type : Header <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology: ASD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 489 @ 1 1/2" | 3645 (3.00") | Passed (13\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Shear (lbs) | 408 @ 10 1/4" | 2501 | Passed (16\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Moment (Ft-lbs) | 1194 @ 5' 1 1/2" | 2569 | Passed (46\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Live Load Defl. (in) | 0.109 @ 5' 1 1/2" | 0.333 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |
| Total Load Defl. (in) | 0.174 @ 5' 1 1/2" | 0.313 | Passed (L/692) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |  |

- Deflection criteria: LL (L/360) and TL (L/5/16").
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1- Trimmer - DF | $3.00^{\prime \prime}$ | $3.00^{\prime \prime}$ | $1.50^{\prime \prime}$ | 182 | 308 | 490 | None |
| 2 - Trimmer - DF | $3.00^{\prime \prime}$ | $3.00^{\prime \prime}$ | $1.50^{\prime \prime}$ | 182 | 308 | 490 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $10^{\prime} 3 \mathrm{Jo} o / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $10^{\prime} 3 \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $10^{\prime} 3^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 5.5 | -- |  |
| 1 - Uniform (PSF) | 0 to $10^{\prime} 3^{\prime \prime}$ | $2^{\prime}$ | 15.0 | 30.0 | Snow |

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Upper Floor, Canopy Cantilever

## 3 piece(s) 1 3/4" x 7 1/4" 2.0E Microllam® LVL



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $3290 @ 4^{\prime} 11 / 2^{\prime \prime}$ | $6379\left(3.00^{\prime \prime}\right)$ | Passed (52\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $1734 @ 4^{\prime} 101 / 4^{\prime \prime}$ | 7232 | Passed (24\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $-3820 @ 4^{\prime} 11 / 2^{\prime \prime}$ | 12273 | Passed (31\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.169 @ 0$ | 0.206 | Passed (2L/584) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | $0.228 @ 0$ | 0.412 | Passed (2L/434) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Overhang deflection criteria: $\operatorname{LL}(2 \mathrm{~L} / 480)$ and $\mathrm{TL}(2 \mathrm{~L} / 240)$.
- Left cantilever length exceeds $1 / 3$ member length or $1 / 2$ back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1 - Stud wall - HF | 3.00" | 3.00 " | 1.55" | 1343 | 1452 | 1144 | 3939 | Blocking |
| 2 - Hanger on $71 / 4$ " HF beam | 3.00" | Hanger ${ }^{1}$ | 1.50 " | 476 | 1519 | -484 | $\begin{gathered} \text { 1995/- } \\ 484 \end{gathered}$ | See note ${ }^{1}$ |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $9^{\prime} 3^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $9^{\prime} 3^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

## Connector: Simpson Strong-Tie

| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 - Face Mount Hanger | HGUS5.50/8 | 4.00 | N/A | $36-10 d$ | $12-10 d$ |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

ForteWEB Software Operator

Job Notes

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## Upper Floor, Floor beam at canopy cantilever

## 1 piece(s) 5 1/4" x 11 7/8" 2.2E Parallam® PSL



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $2126 @ 18^{\prime} 4^{\prime \prime}$ | $6379\left(3.00^{\prime \prime}\right)$ | Passed (33\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $2196 @ 1^{\prime} 53 / 8^{\prime \prime}$ | 12053 | Passed (18\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | 14308 @ $8^{\prime} 3^{\prime \prime}$ | 29854 | Passed (48\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.327 @ 9^{\prime} 111 / 16^{\prime \prime}$ | 0.450 | Passed (L/661) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.478 @ 9^{\prime} 17 / 8^{\prime \prime}$ | 0.900 | Passed (L/452) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1 - Stud wall - HF | 5.50" | 5.50" | 1.50 " | 797 | 1598 | -271 | $\begin{gathered} 2395 /- \\ 271 \end{gathered}$ | Blocking |
| 2-Stud wall - HF | 3.00" | 3.00" | 1.50 " | 728 | 1398 | -213 | $\begin{gathered} 2126 /- \\ 213 \end{gathered}$ | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $18^{\prime} 6{ }^{\prime \prime} 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $18^{\prime} 6{ }^{\prime \prime} 0 / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 0-Self Weight (PLF) | 0 to $18^{\prime} 51 / 2^{\prime \prime}$ | N/A | 19.5 | -- | -- |
| 1 - Uniform (PSF) | 0 to $18^{\prime} 51 / 2^{\prime \prime}$ (Front) | $1^{\prime} 4 \prime$ | 28.0 | 60.0 | - |
| 2 - Point (lb) | $8^{\prime} 3^{\prime \prime}$ (Front) | N/A | 476 | 1519 | -484 |

## Weyerhaeuser Notes




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Upper Floor, Elevator Rim - out of plane
1 piece(s) 1 3/4" x 14" 1.55E TimberStrand ${ }^{\circledR}$ LSL (Plank)

Overall Length: $1^{\prime} 10^{\prime \prime}$


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $172 @ 11 / 2^{\prime \prime}$ | $32550(3.00 ")$ | Passed (1\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $169 @ 43 / 4^{\prime \prime}$ | 2450 | Passed (7\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $92 @ 8 "$ | 1557 | Passed (6\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.004 @ 1011 / 16^{\prime \prime}$ | 0.053 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.004 @ 1011 / 16^{\prime \prime}$ | 0.079 | Passed (L/999+) | -- | $1.0 \mathrm{D} \mathrm{+} \mathrm{1.0} \mathrm{~L} \mathrm{(All} \mathrm{Spans)}$ |

System : Wall
Member Type : Header Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Member has been designed in flat (plank) orientation with vertical (gravity) loads applied to wide strand face.
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Trimmer - DF | 3.00" | 3.00 " | 1.50" | 7 | 165 | 172 | None |
| 2 - Trimmer - DF | 3.00 " | 3.00 " | 1.50" | 7 | 86 | 93 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $1^{\prime} 10^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $1^{\prime} 10^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to $1^{\prime} 10 "$ | N/A | 7.7 | -- |  |
| 1 - Point (Ib) | $8^{\prime \prime}$ | N/A | - | 251 |  |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
| Bykonen Carter Quinn |  |
| (206) 264-7784 |  |
| jaj@bcq-se.com |  |

Upper Floor, Floor: J oist 14' span, typ.
1 piece(s) $\mathbf{1 1 7 / 8 " T J I ® 2 1 0 @ 1 6 " O C}$


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.


- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of $23 / 32$ " Weyerhaeuser Edge ${ }^{T M}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro ${ }^{\text {TM }}$ Rating include: None.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 272 | 389 | 661 | Blocking |
| 2 - Beam - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 272 | 389 | 661 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} 100^{\prime \prime} 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $14^{\prime} 7{ }^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1- Uniform (PSF) | 0 to $14^{\prime} 7^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Default Load |

## Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
| Bykonen Carter Quinn |  |
| (206) 264-7784 |  |
| jaj@bcq-se.com |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Flush Beam <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 10019 @ 12' 7" | 11694 (5.50") | Passed (86\%) | -- | $\begin{array}{\|l} \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ \text { Spans) } \\ \hline \end{array}$ |  |
| Shear (lbs) | 6545 @ 11' 3 1/2" | 16342 | Passed (40\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |  |
| Moment (Ft-lbs) | 24319 @ 6' 8 3/16" | 46854 | Passed (52\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |  |
| Live Load Defl. (in) | 0.223 @ 6' 7 7/16" | 0.306 | Passed (L/658) | -- | $\begin{aligned} & \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \\ & \hline \end{aligned}$ |  |
| Total Load Defl. (in) | 0.358 @ 6' $67 / 8{ }^{\prime \prime}$ | 0.613 | Passed (L/410) | -- | $\qquad$ |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Seismic | Total |  |
| 1-Stud wall - HF | 5.50" | 5.50" | 4.05" | 3506 | 1908 | 4166 | 1044/-1044 | $\begin{gathered} \text { 10624/- } \\ 1044 \end{gathered}$ | Blocking |
| 2-Stud wall - HF | 5.50" | 5.50" | 4.71" | 3766 | 2403 | 4166 | 2526/-2526 | $\begin{gathered} \text { 12861/- } \\ 2526 \end{gathered}$ | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} 11^{\prime \prime} \circ / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $(\mathbf{0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) | Seismic <br> (1.60) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments |  |  |  |  |  |  |

## Weyerhaeuser Notes




 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.weyerhaeuser.com/woodproducts/document-library.
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator
ForteWEB Software Operator
Job Notes

FORTE WEB

## MEMBER REPORT

## Upper Floor, B14 FB at stair, omega

## 1 piece(s) 5 1/4" x 14" 2.0E Parallam® PSL

An excessive uplift of -2160 lbs at support located at $12^{\prime} 7^{\prime \prime}$ failed this product.


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 12008 @ 12' 7" | 18047 (5.50") | Passed (67\%) | -- | $\begin{array}{\|l} \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ \text { Spans) } \\ \hline \end{array}$ |
| Shear (lbs) | 9860 @ 11' 3 1/2" | 22736 | Passed (43\%) | 1.60 | $\begin{aligned} & \text { 1.0 D }+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \end{aligned}$ |
| Moment (Ft-lbs) | 24319 @ 6' 8 3/16" | 46854 | Passed (52\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.292 @ 6' 8 11/16" | 0.306 | Passed (L/503) | -- | $\begin{array}{\|l} \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S}(\mathrm{All} \\ \text { Spans) } \\ \hline \end{array}$ |
| Total Load Defl. (in) | 0.427 @ 6' 7 13/16" | 0.613 | Passed (L/344) | -- | $\begin{aligned} & 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \end{aligned}$ |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

Deflection criteria: LL (L/480) and TL (L/240).

- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Seismic | Total |  |
| 1 - Column - HF | 5.50" | 5.50" | 2.87" | 3506 | 1908 | 4166 | 2611/-2611 | $\begin{gathered} 12191 /- \\ 2611 \end{gathered}$ | Blocking |
| 2-Column - HF | 5.50" | 5.50" | 3.66" | 3766 | 2403 | 4166 | 6314/-6314 | $\begin{gathered} 16649 /- \\ 6314 \end{gathered}$ | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} 11^{\prime \prime} \circ / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ (0.90) \end{gathered}$ | Floor Live (1.00) | Snow <br> (1.15) | Seismic (1.60) | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-Self Weight (PLF) | 0 to 12' $11^{\prime \prime}$ | N/A | 23.0 | -- | -- | -- |  |
| 1 - Uniform (PSF) | 0 to 12' 11" (Front) | 6' 6" | 28.0 | 40.0 | - | - | Default Load |
| 2 - Uniform (PSF) | 0 to 12' 11" (Top) | 21' 6" | 15.0 | - | 30.0 | - |  |
| 3 - Uniform (PSF) | $9^{\prime}$ to 12' 11" (Back) | $2^{\prime}$ | 28.0 | 40.0 | - | - | Default Load |
| 4 - Point (lb) | 9' (Top) | N/A | 240 | 640 | - | - | Stair beam |
| 5 - Point (lb) | 9' (Front) | N/A | - | - | - | 8925 | Hold-down, overstrength $=2.5$ |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

Upper Floor, B14 FB at stair
1 piece(s) 3 1/2" x 14" 1.55E TimberStrand ${ }^{\text {® }}$ LSL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Flush Beam <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 7271 @ 7' 2" | 7796 (5.50") | Passed (93\%) | -- | $\begin{aligned} & 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \\ & \hline \end{aligned}$ |  |
| Shear (lbs) | 3057 @ 5' 10 1/2" | 11646 | Passed (26\%) | 1.15 | 1.0 D + 0.75L + 0.75 S (All Spans) |  |
| Moment (Ft-lbs) | 7915 @ 3' 9 5/8" | 25116 | Passed (32\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |  |
| Live Load Defl. (in) | 0.051 @ 3' 10" | 0.171 | Passed (L/999+) | -- | $\begin{array}{\|l} \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ \text { Spans) } \\ \hline \end{array}$ |  |
| Total Load Defl. (in) | 0.085 @ 3' 9 11/16" | 0.342 | Passed (L/966) | -- | $\begin{aligned} & 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \end{aligned}$ |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- 830 lbs uplift at support located at $7^{\prime} 2^{\prime \prime}$. Strapping or other restraint may be required.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Seismic | Total |  |
| 1 - Stud wall - HF | 5.50" | 5.50" | 3.66 " | 2183 | 1337 | 2419 | 348/-348 | $\begin{gathered} 6287 /- \\ 348 \end{gathered}$ | Blocking |
| 2-Stud wall - HF | 5.50" | 5.50" | 5.13" | 2376 | 1853 | 2419 | 3222/-3222 | $\begin{gathered} 9870 /- \\ 3222 \end{gathered}$ | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $7^{\prime} 6 \mathrm{\prime}$ o/c |  |
| Bottom Edge (Lu) | $7^{\prime} 6 \mathrm{o}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Snow <br> $(\mathbf{1 . 1 5})$ | Seismic <br> $(\mathbf{1 . 6 0})$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Comments |  |  |  |  |  |  |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator
ForteWEB Software Operator

FORTE WEB

## MEMBER REPORT

## Upper Floor, B14 FB at stair, omega

## 1 piece(s) 3 1/2" x 14" 1.55E TimberStrand ${ }^{\text {® }}$ LSL

An excessive uplift of -4212 lbs at support located at 7' $\mathbf{2}^{\prime \prime}$ failed this product.


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 9808 @ 7' 2" | 13956 (5.50") | Passed (70\%) | -- | $\begin{array}{\|l} \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ \text { Spans) } \\ \hline \end{array}$ |
| Shear (lbs) | 4776 @ 5' 10 1/2" | 16203 | Passed (29\%) | 1.60 | $\begin{aligned} & \text { 1.0 D }+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \end{aligned}$ |
| Moment (Ft-lbs) | 7915 @ 3' 9 5/8" | 25116 | Passed (32\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.062 @ 3' 10 3/4" | 0.171 | Passed (L/999+) | -- | $\begin{array}{\|l} \hline 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S}(\mathrm{All} \\ \text { Spans) } \\ \hline \end{array}$ |
| Total Load Defl. (in) | 0.095 @ 3' 10 3/16" | 0.342 | Passed (L/859) | -- | $\begin{aligned} & 1.0 \mathrm{D}+0.525 \mathrm{E}+0.75 \mathrm{~L}+0.75 \mathrm{~S} \text { (All } \\ & \text { Spans) } \end{aligned}$ |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Seismic | Total |  |
| 1-Column - HF | 5.50" | $5.50{ }^{\prime \prime}$ | 2.15" | 2183 | 1337 | 2419 | 871/-871 | $\begin{gathered} \text { 6810/- } \\ 871 \end{gathered}$ | Blocking |
| 2-Column - HF | 5.50" | 5.50" | 3.87" | 2376 | 1853 | 2419 | 8054/-8054 | $\begin{gathered} 14702 /- \\ 8054 \end{gathered}$ | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $7^{\prime} 6 " 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $7^{\prime} 6 " 0 / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ \mathbf{( 0 . 9 0 )} \end{gathered}$ | Floor Live (1.00) | Snow (1.15) | Seismic (1.60) | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to 7' 6" | N/A | 15.3 | -- | -- | -- |  |
| 1 - Uniform (PSF) | 0 to 7' 6" (Front) | $6^{\prime \prime}{ }^{\prime \prime}$ | 28.0 | 40.0 | - | - | Default Load |
| 2 - Uniform (PSF) | 0 to 7' 6" (Top) | 21'6" | 15.0 | - | 30.0 | - |  |
| 3 - Uniform (PSF) | 0 to 7' 6" (Back) | $2^{\prime}$ | 28.0 | 40.0 | - | - | Default Load |
| 4 - Point (lb) | 6' 6" (Top) | N/A | 240 | 640 | - | - | Stair beam |
| 5 - Point (lb) | 6' 6" (Front) | N/A | - | - | - | 8925 | Hold-down, overstrength $=2.5$ |

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Main Framing Key



Main Floor, J1
1 piece(s) 14" TJI® 110 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 839 @ 17' 11 1/2" | 1375 (3.50") | Passed (61\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Shear (lbs) | 797 @ $31 / 2^{\prime \prime}$ | 1860 | Passed (43\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Moment (Ft-lbs) | 3571 @ 9'1" | 3740 | Passed (95\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Live Load Defl. (in) | 0.276 @ 9' 1" | 0.444 | Passed (L/771) | -- | 1.0 D + 1.0 L (All Spans) |  |
| Total Load Defl. (in) | 0.470 @ 9' 1" | 0.887 | Passed (L/454) | -- | 1.0 D + 1.0 L (All Spans) |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 53 | 40 | Passed | -- | -- |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 339 | 484 | 823 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 345 | 493 | 838 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime} 2^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $18^{\prime} 4$ " o/c |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1- Uniform (PSF) | 0 to $18^{\prime} 4^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |

## Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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Main Floor, J2
1 piece(s) 14 " TJ I® 110 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $476 @ 41 / 2^{\prime \prime}$ | $1375(3.50 ")$ | Passed (35\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $434 @ 51 / 2^{\prime \prime}$ | 1860 | Passed (23\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $1077 @ 5^{\prime} 3^{\prime \prime}$ | 3740 | Passed (29\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.032 @ 5^{\prime} 3^{\prime \prime}$ | 0.244 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Building Use : Joist |  |  |  |  |  |
| Building Codential $:$ IBC 2018 |  |  |  |  |  |
| Total Load Defl. (in) | $0.054 @ 5^{\prime} 3^{\prime \prime}$ | 0.488 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 72 | 40 | Passed | -- | -- |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 196 | 280 | 476 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 196 | 280 | 476 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 1 " 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $10^{\prime} 6 " 0 / \mathrm{c}$ |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $10^{\prime} 6^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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Main Floor, J3
1 piece(s) 14" TJI® 110 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 699 @ 4 1/2" | 1375 (3.50") | Passed (51\%) | 1.00 | 1.0 D + 1.0 L (All Spans) |  |
| Shear (lbs) | 657 @ $51 / 2^{\prime \prime}$ | 1860 | Passed (35\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Moment (Ft-lbs) | 2438 @ 7' $81 / 2^{\prime \prime}$ | 3740 | Passed (65\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Live Load Defl. (in) | 0.136 @ 7' 8 1/2" | 0.367 | Passed (L/999+) | -- | 1.0 D + 1.0 L (All Spans) |  |
| Total Load Defl. (in) | 0.231 @ 7' 8 1/2" | 0.733 | Passed (L/763) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 62 | 40 | Passed | -- | -- |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. $8^{\prime}$ o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 288 | 411 | 699 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 288 | 411 | 699 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $15^{\prime} 5^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1- Uniform (PSF) | 0 to $15^{\prime} 5 \prime$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |

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Main Floor, J4
1 piece(s) 11 7/8" $\mathbf{T}$ I © 110 @ $\mathbf{1 6 " O C}$


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 880 @ 4 1/2" | 1375 (3.50") | Passed (64\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Shear (lbs) | 826 @ $51 / 2^{\prime \prime}$ | 1560 | Passed (53\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Moment (Ft-lbs) | 2978 @ 7' 6" | 3160 | Passed (94\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Live Load Defl. (in) | 0.257 @ 7' 6" | 0.356 | Passed (L/664) | -- | 1.0 D + 1.0 L (All Spans) |  |
| Total Load Defl. (in) | 0.378 @ 7' 6" | 0.712 | Passed (L/453) | -- | 1.0 D + 1.0 L (All Spans) |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 59 | 40 | Passed | -- | -- |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 280 | 600 | 880 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 280 | 600 | 880 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime} 2^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $15^{\prime} \mathrm{o} / \mathrm{c}$ |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $15^{\prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

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Main Floor, J5
1 piece(s) 11 7/8"TJI® $360 @ 16 " O C$


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $939 @ 51 / 2^{\prime \prime}$ | $1080\left(1.75^{\prime \prime}\right)$ | Passed (87\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $939 @ 51 / 2^{\prime \prime}$ | 1705 | Passed (55\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $3755 @ 8^{\prime} 51 / 2^{\prime \prime}$ | 6180 | Passed (61\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.283 @ 8^{\prime} 51 / 2^{\prime \prime}$ | 0.400 | Passed (L/677) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.416 @ 8^{\prime} 51 / 2^{\prime \prime}$ | 0.800 | Passed (L/462) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 56 | 40 | Passed | -- | -- |

System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. $8^{\prime}$ o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $117 / 8{ }^{\prime \prime} \mathrm{HF}$ beam | 5.50" | Hanger ${ }^{1}$ | 1.75" / - 2 | 316 | 677 | 993 | See note ${ }^{1}$ |
| 2 - Stud wall - HF | 3.50" | 3.50" | 1.75" | 306 | 657 | 963 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.
- 2 Required Bearing Length / Required Bearing Length with Web Stiffeners

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} 9{ }^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $16^{\prime} 3^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.
-Maximum allowable bracing intervals based on applied load.

$|$| Connector: Simpson Strong-Tie |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| 1 - Face Mount Hanger | IUS2.37/11.88 | 2.00 | N/A | 10-10d | 2-Strong-Grip |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Load | Location | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $16^{\prime} 8^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

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Job Notes

Main Floor, J6


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System: Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1080 @ 4 1/2" | 3010 (3.50") | Passed (36\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Shear (lbs) | 1027 @ $51 / 2^{\prime \prime}$ | 3410 | Passed (30\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Moment (Ft-lbs) | 4578 @ 9' 2 1/2" | 12360 | Passed (37\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |
| Live Load Defl. (in) | 0.217 @ 9' $21 / 2^{\prime \prime}$ | 0.442 | Passed (L/977) | -- | 1.0 D + 1.0 L (All Spans) |  |
| Total Load Defl. (in) | 0.318 @ 9' $21 / 2^{\prime \prime}$ | 0.883 | Passed (L/666) | -- | 1.0 D + 1.0 L (All Spans) |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 61 | 40 | Passed | -- | -- |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. $8^{\prime}$ o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 344 | 737 | 1081 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 344 | 737 | 1081 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 3^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $18^{\prime} 5^{\prime \prime} \circ / \mathrm{c}$ |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $18^{\prime} 5^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Floor <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 592 @ 4 1/2" | 1375 (3.50") | Passed (43\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Shear (lbs) | 538 @ $51 / 2^{\prime \prime}$ | 1560 | Passed (34\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Moment (Ft-lbs) | 1278 @ 5' 1/2" | 3160 | Passed (40\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Live Load Defl. (in) | 0.056 @ 5' 1/2" | 0.233 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Total Load Defl. (in) | 0.083 @ 5' 1/2" | 0.467 | Passed (L/999+) | -- | 1.0 D + 1.0 L (All Spans) |  |  |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 71 | 40 | Passed | -- | -- |  |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 188 | 403 | 591 | Blocking |
| 2-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 188 | 403 | 591 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $5^{\prime} 1^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $10^{\prime} 1$ " o/c |  |

-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $10^{\prime} 1^{\prime \prime}$ | $16^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

## Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
| Bykonen Carter Quinn |  |
| (206) 264-7784 |  |
| jaj@bcq-se.com |  |

Main Floor, J8
1 piece(s) 14" TJI® 110 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $272 @ 21 / 2^{\prime \prime}$ | $1375(3.50 ")$ | Passed (20\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $246 @ 31 / 2^{\prime \prime}$ | 1860 | Passed (13\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $353 @ 3^{\prime}$ | 3740 | Passed (9\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.006 @ 3^{\prime}$ | 0.140 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Building Use : Joist |  |  |  |  |  |
| Building Codential $:$ IBC 2018 |  |  |  |  |  |
| Total Load Defl. (in) | $0.009 @ 3^{\prime}$ | 0.279 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| TJ-Pro ${ }^{\text {TM }}$ Rating | 78 | 40 | Passed | -- | -- |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge ${ }^{\text {TM }}$ Panel ( 24 " Span Rating) that is glued and nailed down.
- Additional considerations for the $\mathrm{TJ}-\mathrm{Pro}^{T M}$ Rating include: $5 / 8^{\prime \prime}$ Gypsum ceiling, bridging or blocking at max. 8' o.c., Perpendicular Partitions, Pour Flooring Overlay.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 112 | 160 | 272 | Blocking |
| 2 - Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.75^{\prime \prime}$ | 112 | 160 | 272 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $6^{\prime} 0 / \mathrm{c}$ |  |

$\bullet$-TJI joists are only analyzed using Maximum Allowable bracing solutions.

- Maximum allowable bracing intervals based on applied load.

| Vertical Load | Location | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1- Uniform (PSF) | 0 to $6 '$ | $16^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
| Bykonen Carter Quinn |  |
| (206) 264-7784 |  |
| jaj@bcq-se.com |  |

Main Floor, B9
1 piece(s) 3 1/2" x 14" 1.55E TimberStrand® LSL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $448 @ 2^{\prime \prime}$ | $4961(3.50 ")$ | Passed (9\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $128 @ 1^{\prime} 51 / 2^{\prime \prime}$ | 10127 | Passed (1\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $386 @ 2^{\prime} 1 / 2^{\prime \prime}$ | 21840 | Passed (2\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.001 @ 2^{\prime} 1 / 2^{\prime \prime}$ | 0.094 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.002 @ 2^{\prime} 1 / 2^{\prime \prime}$ | 0.188 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Available | Required | Dead | Floor Live | Total | Accessories |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 203 | 245 | 448 | Blocking |
| 2 - Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 219 | 265 | 484 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} 3 \prime \prime 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $4^{\prime} 3 \prime$ " $0 / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to 4' $3^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 15.3 | -- |  |
| 1 - Uniform (PSF) | 0 to 4' 3' (Front) | $3^{\prime}$ | 28.0 | 40.0 | Floor Load |

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| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Jane Johnson |  |
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| (206) 264-7784 |  |
| jaj@bcq-se.com |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $1665 @ 2 "$ | $4961(3.50 ")$ | Passed (34\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $1463 @ 1^{\prime} 3 / 4^{\prime \prime}$ | 6151 | Passed (24\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $6278 @ 6^{\prime} 95 / 8^{\prime \prime}$ | 11204 | Passed (56\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.427 @ 8^{\prime} 9 "$ | 0.446 | Passed (L/502) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.785 @ 8^{\prime} 91 / 8^{\prime \prime}$ | 0.892 | Passed (L/273) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 749 | 917 | 1666 | Blocking |
| 2-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 533 | 622 | 1155 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $18^{\prime} 11^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $18^{\prime} 4 \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0-Self Weight (PLF) | 0 to $18^{\prime} 4^{\prime \prime}$ | N/A | 9.4 | -- |  |
| 1- Uniform (PSF) | 0 to $5^{\prime} 11^{\prime \prime}$ (Front) | $2^{\prime} 8^{\prime \prime}$ | 28.0 | 40.0 | Floor Load |
| 2- Uniform (PSF) | $5^{\prime} 11^{\prime \prime}$ to $18^{\prime} 4 \prime \prime$ (Front) | $1^{\prime} 4 \prime$ | 28.0 | 40.0 | Floor Load |
| 3 - Point (lb) | $5^{\prime} 11^{\prime \prime}$ (Front) | N/A | 203 | 245 | Linked from: B9, <br> Support 1 |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator
ForteWEB Software Operator


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $26087 @ 4 "$ | 39875 (5.50") | Passed (65\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $25177 @ 51 / 2^{\prime \prime}$ | 104250 | Passed (24\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $151607 @ 12^{\prime} 113 / 16^{\prime \prime}$ | 177019 | Passed (86\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.545 @ 12^{\prime} 411 / 16^{\prime \prime}$ | 0.606 | Passed (L/534) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.865 @ 12^{\prime} 413 / 16^{\prime \prime}$ | 1.212 | Passed (L/336) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Bearing reinforcement may be required for support located at 4 ".
- Bearing reinforcement may be required for support located at $24^{\prime} 7{ }^{\prime \prime}$.
- Applicable calculations are based on ANSI/AISC 360-16.
- A lateral-torsional buckling factor $(\mathrm{Cb})$ of 1.0 has been assumed.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1- Column - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | 9581 | 16506 | 26087 | Blocking |
| 2 - Column - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | 9177 | 15175 | 24352 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :--- | :--- |
| Top Edge (Lu) | End Bearing Points |  |
| Bottom Edge (Lu) | End Bearing Points |  |


| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ \mathbf{( 0 . 9 0 )} \end{gathered}$ | Floor Live (1.00) | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to 24' $11{ }^{\prime \prime}$ | N/A | 61.0 | -- |  |
| 1 - Uniform (PSF) | 0 to 24' 11" | 9' 2 " | 28.0 | 40.0 | Floor Load |
| 2 - Tapered (PSF) | 0 to 7' 3" | 5' 6" to 9' | 28.0 | 60.0 | Deck Load |
| 3 - Tapered (PSF) | $7{ }^{\prime \prime} 3^{\prime \prime}$ to $24{ }^{\prime \prime} 11^{\prime \prime}$ | $9^{\prime}$ to 0 | 28.0 | 60.0 | Deck Load |
| 4-Uniform (PSF) | 0 to 24' 11" | 9' ${ }^{\prime \prime}$ | 28.0 | 60.0 | Upper Floor Deck Load |
| 5 - Point (lb) | 20'8" | N/A | 749 | 917 | Linked from: B10, Support 1 |

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ForteWEB Software Operator

## 1 piece(s) W12X53 (A992) ASTM Steel



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $17179 @ 18^{\prime} 1^{\prime \prime}$ | $22275\left(5.500^{\prime \prime}\right)$ | Passed (77\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (Ibs) | $16282 @ 17^{\prime} 111 / 2^{\prime \prime}$ | 83490 | Passed (20\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $124292 @ 10^{\prime}$ | 161513 | Passed (77\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.289 @ 9^{\prime} 415 / 16^{\prime \prime}$ | 0.444 | Passed (L/738) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.465 @ 9^{\prime} 415 / 16^{\prime \prime}$ | 0.887 | Passed (L/458) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Bearing reinforcement may be required for point load located at $10^{\prime}$.
- Applicable calculations are based on ANSI/AISC 360-16.
- A lateral-torsional buckling factor $(\mathrm{Cb})$ of 1.0 has been assumed.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $5.50 "$ | 5418 | 8623 | 57 | 14098 | Blocking |
| 2-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $5.50 "$ | 6794 | 10385 | 633 | 17812 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :--- | :--- |
| Top Edge (Lu) | End Bearing Points |  |
| Bottom Edge (Lu) | End Bearing Points |  |


| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ (0.90) \end{gathered}$ | Floor Live (1.00) | $\begin{aligned} & \text { Snow } \\ & \text { (1.15) } \end{aligned}$ | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to 18' ${ }^{\prime \prime}$ | N/A | 53.0 | -- | -- |  |
| 1 - Uniform (PSF) | 0 to 10' | $2 '$ | 28.0 | 60.0 | - | Deck Load |
| 2 - Uniform (PSF) | $10^{\prime}$ to $18^{\prime} 5^{\prime \prime}$ | $1 '$ | 28.0 | 40.0 | - | Floor Load |
| 3 - Uniform (PSF) | $10^{\prime}$ to $8^{\prime \prime} 5^{\prime \prime}$ | $1 '$ | 28.0 | 60.0 | - | Deck Load |
| 4 - Point (lb) | 18' | N/A | 298 | 220 | 330 | Linked from: B6, Support 1 |
| 5 - Point (lb) | 12' 6" | N/A | 163 | 120 | 180 | Linked from: B12, Support 1 |
| 6 - Point (lb) | 18' | N/A | 163 | 120 | 180 | Linked from: B12, Support 2 |
| 7 - Point (lb) | 10' | N/A | 9581 | 16506 | - | Linked from: B11, Support 1 |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 2628 @ 4" | 6683 (5.50") | Passed (39\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $2524 @ 1^{\prime} 23 / 4^{\prime \prime}$ | 3191 | Passed (79\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | $3079 @ 1 ' 61 / 2^{\prime \prime}$ | 3833 | Passed (80\%) | 1.15 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.038 @ 33^{\prime} 23 / 16^{\prime \prime}$ | 0.158 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | $0.069 @ 3 ' 25 / 16^{\prime \prime}$ | 0.317 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1 - Stud wall - HF | 5.50" | 5.50 " | 2.16" | 1175 | 814 | 1123 | 3112 | Blocking |
| 2 - Stud wall - HF | 5.50" | 5.50" | 1.50 " | 396 | 335 | 265 | 996 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $7^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $7^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

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 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.weyerhaeuser.com/woodproducts/document-library.
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1330 @ 4" | 6683 (5.50") | Passed (20\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | 388 @ 1'3/4" | 2175 | Passed (18\%) | 1.00 | 1.0 D + 1.0 L (All Spans) |
| Moment (Ft-lbs) | 603 @ 1' 6" | 2234 | Passed (27\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | 0.003 @ 1' 6" | 0.058 | Passed (L/999+) | -- | 1.0 D + 1.0 L (All Spans) |
| Total Load Defl. (in) | 0.005 @ 1' 6" | 0.117 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | 5.50" | 5.50" | 1.50" | 553 | 777 | 1330 | Blocking |
| 2 - Stud wall - HF | 5.50" | 5.50" | 1.50" | 553 | 777 | 1330 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $3^{\prime}$ o/c |  |
| Bottom Edge (Lu) | $3^{\prime}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $3^{\prime}$ | N/A | 5.5 | -- |  |
| 1 - Uniform (PLF) | 0 to 3' (Front) | N/A | 147.0 | 210.0 | Linked from: J2, <br> Support 2 |
| 2 - Uniform (PLF) | 0 to 3' (Front) | N/A | 216.0 | 308.3 | Linked from: J3, <br> Support 1 |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 5181 @ 4" | 11694 (5.50") | Passed (44\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $4197 @ 1^{\prime} 53 / 8^{\prime \prime}$ | 12053 | Passed (35\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $18063 @ 7^{\prime} 71 / 2^{\prime \prime}$ | 29854 | Passed (61\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.304 @ 7^{\prime} 71 / 2^{\prime \prime}$ | 0.365 | Passed (L/575) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.459 @ 7^{\prime} 71 / 2^{\prime \prime}$ | 0.729 | Passed (L/381) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $2.44 "$ | 1750 | 3431 | 5181 | Blocking |
| 2-Stud wall - HF | $5.50^{\prime \prime}$ | $5.50^{\prime \prime}$ | $2.44^{\prime \prime}$ | 1750 | 3431 | 5181 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $15^{\prime} 3^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $15^{\prime} \mathrm{J}$ " /c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $15^{\prime} 3^{\prime \prime}$ | N/A | 19.5 | -- |  |
| 1- Uniform (PSF) | 0 to $15^{\prime} 3^{\prime \prime}$ (Front) | $7^{\prime} 6^{\prime \prime}$ | 28.0 | 60.0 | Deck Load |

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Main Floor, Entry canopy - Green roof, 65 psf
1 piece(s) $2 \times 10$ DF No. 2 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Roof <br> Member Type : Joist <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD <br> Member Pitch : 0.25/12 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 831 @ $31 / 2^{\prime \prime}$ | 1406 (1.50") | Passed (59\%) | -- | 1.0 D + 1.0 S (All Spans) |  |  |
| Shear (lbs) | 718 @ 1'3/4" | 1915 | Passed (38\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |  |
| Moment (Ft-lbs) | 2355 @ 5' 11 1/2" | 2334 | Passed (101\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |  |  |
| Live Load Defl. (in) | 0.094 @ 5' 11 1/2" | 0.567 | Passed (L/999+) | -- | 1.0 D + 1.0 S (All Spans) |  |  |
| Total Load Defl. (in) | 0.344 @ 5' 11 1/2" | 0.756 | Passed (L/395) | -- | 1.0 D + 1.0 S (All Spans) |  |  |

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Available | Required | Dead | Snow | Total | Accessories |  |
| 1-Hanger on 9 1/4" HF beam | $3.50^{\prime \prime}$ | Hanger $^{1}$ | $1.50^{\prime \prime}$ | 636 | 238 | 874 | See note ${ }^{1}$ |
| 2 - Beam - HF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 627 | 235 | 862 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | 6 o o/c |  |
| Bottom Edge (Lu) | $11^{\prime} 7 \mathrm{c} \circ / \mathrm{c}$ |  |

$\bullet$ Maximum allowable bracing intervals based on applied load.

## Connector: Simpson Strong-Tie

| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - Face Mount Hanger | LRU28Z | $1.94 "$ | N/A | $6-10 \mathrm{~d}$ | $5-10 \mathrm{~d}$ |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Load | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $11^{\prime} 10^{\prime \prime}$ | $16^{\prime \prime}$ | 80.0 | 30.0 | Green roof 50 psf |

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J ob Notes


## Main Floor, DB Green roof 65 psf

## 1 piece(s) $\mathbf{6 \times 1 0} \mathbf{D F}$ No. 1



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Roof <br> Member Type : Drop Beam <br> Building Use : Residential <br> Building Code : IBC 2018 <br> Design Methodology : ASD <br> Member Pitch : 0/12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 4050 @ 9 3/4" | 7796 (3.50") | Passed (52\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Shear (lbs) | 2728 @ 1' 9" | 6810 | Passed (40\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Moment (Ft-lbs) | 7580 @ 5' 4 1/4" | 10703 | Passed (71\%) | 1.15 | 1.0 D + 1.0 S (Alt Spans) |  |
| Live Load Defl. (in) | 0.048 @ 5' 3 15/16" | 0.451 | Passed (L/999+) | -- | 1.0 D + 1.0 S (Alt Spans) |  |
| Total Load Defl. (in) | 0.176 @ 5' 4" | 0.601 | Passed (L/615) | -- | 1.0 D + 1.0 S (Alt Spans) |  |

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1-Stud wall - HF | 3.50 " | 3.50" | 1.82" | 2965 | 1085 | 4050 | Blocking |
| 2 - Stud wall - HF | 3.50 " | 3.50 " | 1.58" | 2567 | 943 | 3510 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $10^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $10^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $10^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.2 | -- |  |
| 1 - Uniform (PSF) | 0 to $10^{\prime}$ (Front) | $6^{\prime} 9 \prime$ | 80.0 | 30.0 | Default Load |

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## Main Floor, Garage Flush Header

## 1 piece(s) 5 1/4" x 11 7/8" 2.2E Parallam® PSL



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $4737 @ 11 / 2^{\prime \prime}$ | $6379\left(3.00^{\prime \prime}\right)$ | Passed (74\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $3891 @ 1^{\prime} 27 / 8^{\prime \prime}$ | 12053 | Passed (32\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $17513 @ 8^{\prime} 31 / 16^{\prime \prime}$ | 29854 | Passed (59\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.437 @ 99^{\prime}$ | 0.456 | Passed (L/501) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.673 @ 9^{\prime} 1 / 8^{\prime \prime}$ | 0.913 | Passed (L/325) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - HF | $3.00 "$ | $3.00 "$ | $2.23^{\prime \prime}$ | 1630 | 3107 | 4737 | Blocking |
| 2-Stud wall - HF | $3.00 "$ | $3.00^{\prime \prime}$ | $1.50 "$ | 1061 | 1888 | 2949 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $18^{\prime} 6 \mathrm{\prime} \mathrm{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $18^{\prime} 6 \mathrm{o} \circ \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $18^{\prime} 6^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 19.5 | -- |  |
| 1 - Tapered (PSF) | 0 to $18^{\prime} 6^{\prime \prime}$ (Front) | $7^{\prime} 9^{\prime \prime}$ to $1^{\prime} 3^{\prime \prime}$ | 28.0 | 60.0 | Deck |

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## ATC Hazards by Location

## Search Information

| Address: | 7221 78th Ave SE, Mercer Island, WA 98040, USA |
| :--- | :--- |
| Coordinates: | $47.560961,-122.225477$ |
| Elevation: | 268 ft |
| Timestamp: | $2021-12-28$ T00:19:49.647Z |
| Hazard Type: | Seismic |
| Reference Document: | ASCE7-16 |
| Risk Category: | II |
| Site Class: | D |



## Basic Parameters

| Name | Value | Description |
| :--- | :--- | :--- |
| $\mathrm{S}_{\mathrm{S}}$ | 1.439 | MCE $_{\mathrm{R}}$ ground motion (period=0.2s) |
| $\mathrm{S}_{1}$ | 0.5 | MCE $_{\mathrm{R}}$ ground motion (period=1.0s) |
| $\mathrm{S}_{\mathrm{MS}}$ | 1.439 | Site-modified spectral acceleration value |
| $\mathrm{S}_{\mathrm{M} 1}$ | $*$ null | Site-modified spectral acceleration value |
| $\mathrm{S}_{\mathrm{DS}}$ | 0.959 | Numeric seismic design value at 0.2 s SA |
| $\mathrm{S}_{\mathrm{D} 1}$ | * null | Numeric seismic design value at 1.0 s SA |

* See Section 11.4.8


## -Additional Information

| Name | Value | Description |
| :---: | :---: | :---: |
| SDC | * null | Seismic design category |
| $\mathrm{F}_{\mathrm{a}}$ | 1 | Site amplification factor at 0.2 s |
| $\mathrm{F}_{\mathrm{v}}$ | * null | Site amplification factor at 1.0 s |
| $\mathrm{CR}_{S}$ | 0.902 | Coefficient of risk (0.2s) |
| $\mathrm{CR}_{1}$ | 0.898 | Coefficient of risk (1.0s) |
| PGA | 0.616 | $\mathrm{MCE}_{\mathrm{G}}$ peak ground acceleration |
| $\mathrm{F}_{\mathrm{PGA}}$ | 1.1 | Site amplification factor at PGA |
| PGA ${ }_{M}$ | 0.678 | Site modified peak ground acceleration |
| $\mathrm{T}_{\mathrm{L}}$ | 6 | Long-period transition period (s) |
| SsRT | 1.439 | Probabilistic risk-targeted ground motion (0.2s) |
| SsUH | 1.595 | Factored uniform-hazard spectral acceleration (2\% probability of exceedance in 50 years) |
| SsD | 3.957 | Factored deterministic acceleration value (0.2s) |
| S1RT | 0.5 | Probabilistic risk-targeted ground motion (1.0s) |
| S1UH | 0.557 | Factored uniform-hazard spectral acceleration (2\% probability of exceedance in 50 years) |
| S1D | 1.551 | Factored deterministic acceleration value (1.0s) |
| PGAd | 1.333 | Factored deterministic acceleration value (PGA) |

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

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Hazard loads are provided by the U.S. Geological Survey Seismic Design Web Services.
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report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.

## Search Information

| Address: | 7221 78th Ave SE, Mercer Island, WA 98040, USA |
| :--- | :--- |
| Coordinates: | $47.560961,-122.225477$ |
| Elevation: | 268 ft |
| Timestamp: | $2021-12-28$ T00:22:17.892Z |
| Hazard Type: | Wind |



| ASCE 7-16 |  |
| :---: | :---: |
| MRI 10-Year | 67 mph |
| MRI 25-Year | 73 mph |
| MRI 50-Year | 78 mph |
| MRI 100-Year | 83 mph |
| Risk Category I | 92 mph |
| Risk Category II | 97 mph |
| Risk Category III | 104 mph |
| Risk Category IV | 108 mph |

ASCE 7-10

MRI 10-Year .-.............................. 72 mph

ASCE 7-05

ASCE 7-05 Wind Speed
85 mph

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

## Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area - in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.
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LATERAL KEY - UPPER FLOOR $3 \quad 4 \quad 5$



1. Shear wall demands have been increased where seismic controls design and $\mathrm{h} / \mathrm{L}$ is greater than $2: 1$ per SDPWS Table 4.3.4. Where wind controls design, shearwall demands have been decreased $40 \%$ per IBC 2306.3 .

| UPPER |  | $\begin{array}{r} \text { WIND TRIB }= \\ 0.6 \mathrm{~W}(\mathrm{k})= \\ \text { SEISMIC TRIB }= \end{array}$ | 11\% |  | $\Sigma \mathrm{LL}=$ | 14.25 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1.30 |  |  |  |  |  |  |  |  |  |
|  |  |  | 11\% |  |  |  |  |  |  |  |  |  |
|  |  | $0.7 \mathrm{E}(\mathrm{k})=$ | 0.96 |  |  |  |  |  |  | Wall weight |  |  |
| Segment Count | HT (ft) | LENGTH (ft) | h/L | $2 /(h / L)^{1}$ | 0.6 W (plf) | 0.7 E (plf) | sw | SW Cap (plf) | Tension (k) | 0.6-0.14Sds | $[0.6-0.14 \mathrm{Sd} s] \mathrm{D}$ <br> (k) | Net T (k) |
| 1 | 9.4 | 14.3 | 0.66 | 1.00 | 65 | 67 | SW 1 | 240 | 0.6 | 0.47 | 0.6 | 0.3 |




| UPPER |  | WIND TRIB $=$ | 17\% |  | $\Sigma \mathrm{L}=$ | 24.00 |  |  |  | Wall weight |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0.6 \mathrm{~W}(\mathrm{k})=$ | 2.01$17 \%$ |  |  |  |  |  |  |  |  |  |
|  |  | SEISMIC TRIB = |  |  |  |  |  |  |  |  |  |  |
|  |  | $0.7 \mathrm{E}(\mathrm{k})=$ | 1.48 |  |  |  |  |  |  |  |  |  |
| Segment Count | HT (ft) | LENGTH (ft) | h/L | 2/(h/L) ${ }^{1}$ | 0.6 W (plf) | 0.7 E (plf) | SW | SW Cap (plf) | Tension (k) | 0.6-0.14Sds | $[0.6-0.14 \mathrm{Sds}] \mathrm{D}$ <br> (k) | Net T (k) |
| 1 | 9.4 | 24.0 | 0.39 | 1.00 | 60 | 62 | SW 1 | 240 | 0.6 | 0.47 | 1.0 | 0.1 |
| MAIN |  | WIND TRIB $=$ | 43\% |  | $\Sigma \mathrm{L}=$ | 9.00 |  |  |  |  |  |  |
|  |  | $0.6 \mathrm{~W}(\mathrm{k})=$ | 7.98 |  |  |  |  |  |  |  |  |  |
|  |  | SEISMIC TRIB = | 35\% |  |  |  |  |  |  |  |  |  |
|  |  | $0.7 \mathrm{E}(\mathrm{k})=$ | 2.98 |  |  |  |  |  |  | Wall weight |  |  |
| Segment Count | HT (ft) | LENGTH (ft) | h/L | $2 /(\mathrm{h} / \mathrm{L})^{1}$ | 0.6 W (plf) | 0.7 E (plf) | SW | sW Cap (plf) | Tension (k) | 0.6-0.14Sds | $[0.6-0.14 \mathrm{Sds}] \mathrm{D}$ <br> (k) | Net T (k) |
| 1 | 9.4 | 9.0 | 1.04 | 1.00 | 633 | 331 | SW 4 | 705 | 5.9 | 0.47 | 0.4 | 5.7 |

1. Shear wall demands have been increased where seismic controls design and $h / L$ is greater than 2:1 per SDPWS Table 4.3.4. Where wind controls design, shearwall demands have been decreased $40 \%$ per IBC 2306.3.

| ROOF |  | $\begin{array}{r} \text { WIND TRIB }= \\ 0.6 \mathrm{~W}(\mathrm{k})= \end{array}$ | 22\% |  | $\Sigma \mathrm{L}=$ | 11.30 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.99 |  |  |  |  |  |  |  |  |  |
|  |  | SEISMIC TRIB = | 22\% |  |  |  |  |  |  |  |  |  |
|  |  | $0.7 \mathrm{E}(\mathrm{k})=$ | 0.99 |  |  |  |  |  |  |  | Wall weight |  |
| Segment Count | HT (ft) | LENGTH (ft) | h/L | $2 /(\mathrm{h} / \mathrm{L})^{1}$ | 0.6W (plf) | 0.7 E (plf) | SW | SW Cap <br> (plf) | Tension (k) | 0.6-0.14Sds | $\begin{gathered} {[0.6-0.14 \mathrm{Sds}] \mathrm{D}} \\ (\mathrm{k}) \\ \hline \end{gathered}$ | Net T (k) |
| 1 | 10.2 | 11.3 | 0.90 | 1.00 | 63 | 87 | SW 1 | 240 | 0.9 | 0.47 | 0.5 | 0.6 |
| Concrete |  |  |  |  |  |  |  |  |  |  |  |  |


| ROOF |  | WIND TRIB $=$ | 78\% |  | $\Sigma \mathrm{L}=$ | 14.30 |  |  |  | Wall weight |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0.6 \mathrm{~W}(\mathrm{k})=$ | 3.51 |  |  |  |  |  |  |  |  |  |
|  |  | $\begin{aligned} & \text { SEISMIC TRIB }= \\ & 0.7 \mathrm{E}(\mathrm{k})= \end{aligned}$ | 78\% |  |  |  |  |  |  |  |  |  |
|  |  |  | 3.51 |  |  |  |  |  |  |  |  |  |
| Segment Count | HT (ft) | LENGTH (ft) | h/L | $2 /(\mathrm{h} / \mathrm{L})^{1}$ | 0.6 W (plf) | 0.7 E (plf) | SW | SW Cap <br> (plf) | Tension (k) | 0.6-0.14Sds | $\begin{gathered} {[0.6-0.14 \mathrm{Sds}] \mathrm{D}} \\ (\mathrm{k}) \end{gathered}$ | Net T (k) |
| 1 | 10.2 | 9.5 | 1.07 | 1.00 | 175 | 245 | SW 2 | 355 | 2.5 | 0.47 | 0.5 | 2.3 |
| 1 | 10.2 | 4.8 | 2.13 | 0.94 | 175 | 261 | SW 2 | 355 | 2.5 | 0.47 | 0.2 | 2.4 |
| UPPER |  | WIND TRIB $=$ | 50\% |  | $\Sigma \mathrm{L}=$ | 36.50 |  |  |  |  |  |  |
|  |  | $0.6 \mathrm{~W}(\mathrm{k})=$ | 7.71 |  |  |  |  |  |  |  |  |  |
|  |  | SEISMIC TRIB $=$ | 50\% |  |  |  |  |  |  |  |  |  |
|  |  | $0.7 \mathrm{E}(\mathrm{k})=$ | 7.85 |  |  |  |  |  |  | Wall weight |  |  |
| Segment Count | HT (ft) | LENGTH (ft) | h/L | $2 /(\mathrm{h} / \mathrm{L})^{1}$ | 0.6 W (plf) | 0.7 E (plf) | SW | SW Cap <br> (plf) | Tension (k) | 0.6-0.14Sds | $[0.6-0.14 \mathrm{Sds}] \mathrm{D}$ <br> (k) | Net T (k) |
| 1 | 9.4 | 24.5 | 0.38 | 1.00 | 151 | 215 | SW 1 | 240 | 2.0 | 0.47 | 1.1 | 1.5 |
| 1 | 9.4 | 12.0 | 0.78 | 1.00 | 151 | 215 | SW 1 | 240 | 2.0 | 0.47 | 0.5 | 1.8 |
| Concrete |  |  |  |  |  |  |  |  |  |  |  |  |


| OPEN FRONT |  | Mmax |
| :---: | :---: | :---: |
|  | $\mathrm{D} / 2 \mathrm{ft})$ | (k-ft) |
| $0.6 \mathrm{~W}(\mathrm{k})=$ | 12.25 | 42.95 |
| 0.7 E (k) | 12.2 | 42.9 |

Mmax
(k-ft)
42.95
42.94

|  |  |  |  |  | Bottom Plate Attachment |  |  | $\begin{gathered} \hline \text { Capacity } \\ \text { (plf) } \\ \text { (Seismic) } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mark | Sheathing | Blck'g | Panel Nailing ${ }^{1}$ | Attachment to top plate ${ }^{3}$ | Rim <br> Joist Req'd | Nailing to ${ }^{4}$ wood below | A. Bolts to concrete below |  |
| SW 1 | 15/32" APA Sheathing | Yes | 8d @ 6"oc | CLIP @ 24"oc | 2 x or $13 / 4$ " LSL | 16d @ 6"oc | 5/8" @ 48"oc | 240 |
| SW 2 | 15/32" APA Sheathing | Yes | 8d @ 4"oc ${ }^{2}$ | CLIP @ 20"oc | $2 x$ or $13 / 4$ " LSL | 16d @ 43/4"oc | 5/8" @ 48"oc | 355 |
| SW x | 15/32" APA Sheathing | Yes | 8d @ 3"oc ${ }^{2}$ | CLIP @ 16"oc | 2 x or $13 / 4$ " LSL | 16d @ 33/4"oc | 5/8" @ 36"oc | 455 |
| SW 3 | 15/32" APA Sheathing | Yes | 8d @ 2"oc ${ }^{2}$ | CLIP @ 12"oc | 4 x or $31 / 2^{\prime \prime}$ LSL | (2) Rows ${ }^{6}$ 16d @ 53/4"oc | 5/8" @ 24"oc | 595 |
| SW 4 | 15/32" APA Sheathing Each Side | Yes | 8d @ 4"oc² | CLIP @ 9"oc | 4 x or $31 / 2$ " LSL | (2) Rows ${ }^{6}$ <br> 16d @ 43/4"oc | 5/8" @ 24"oc | 705 |

${ }^{1}$ Nails shall be 8d box. Nailing applies to all panel edges (block all unsupported panel edges), top \& bottom plates and blocking. Nail to intermediate framing members w/ 8d @ 12"oc. (Note: where stud spacing is $24^{\prime \prime} \mathrm{oc}$, nail to intermediate framing members with $8 \mathrm{~d} @ 6 " \mathrm{oc}$.)
${ }^{2}$ Framing at adjoining panel edges shall be 3 -inch nominal or wider and nails shall be staggered.
${ }^{3}$ Clip shall be either A35, LTP4.
${ }^{4}$ Nails shall be 16 d box ( $0.135 \emptyset \times 31 / 2$ ") or 10 d common ( $0.148 \emptyset \times 31 / 2$ ") Screws shall be Simpson SDS25412 (1/4"Øx4½"min).
${ }^{5}$ Provide $3 " x 3 " x 0.229$ " plate washer at all anchor bolts. Anchor bolts shall be positioned such that plate edge of plate washer is with $1 / 2$ " of the edge of the bottom plate.
(Plate washers may be diagonally slotted with a width of up to $13 / 16$ " and a length not to exceed $13 / 4$ ")
${ }^{6}$ Rows must be offset at least $1 / 2$ " and staggered.
${ }^{7}$ Alternate plate washers to provide $1 / 2^{\prime \prime}$ dimension on each side fo the shearwall.

# SIMPSON Anchor Designer ${ }^{\text {TM }}$ <br> Strongtie <br> Software <br> Version 2.8.7094.0 

| Company: |  | Date: | $2 / 4 / 2022$ |
| :--- | :--- | :--- | :--- |
| Engineer: |  | Page: | $1 / 5$ |
| Project: |  |  |  |
| Address: |  |  |  |
| Phone: |  |  |  |
| E-mail: |  |  |  |

## 1.Project information

## Customer company:

Customer contact name:
Customer e-mail:
Comment:

## 2. Input Data \& Anchor Parameters

## General

Design method:ACI 318-14
Units: Imperial units

## Anchor Information:

Anchor type: Cast-in-place
Material: AB
Diameter (inch): 0.875
Effective Embedment depth, hef (inch): 9.000
Anchor category: -
Anchor ductility: Yes
$\mathrm{h}_{\text {min }}$ (inch): 11.38
$\mathrm{C}_{\text {min }}$ (inch): 1.75
$\mathrm{S}_{\text {min }}$ (inch): 3.50

Project description:
Location:
Fastening description:

## Base Material

Concrete: Normal-weight
Concrete thickness, h (inch): 12.00
State: Cracked
Compressive strength, $\mathrm{f}^{\prime} \mathrm{c}$ (psi): 2500
$\psi_{\mathrm{c}, \mathrm{V},} 1.0$
Reinforcement condition: A tension, A shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: Yes
Ignore concrete breakout in tension: No
Ignore concrete breakout in shear: No
Ignore 6do requirement: Yes
Build-up grout pad: No

## Recommended Anchor

Anchor Name: PAB Pre-Assembled Anchor Bolt - PAB7 (7/8"Ø)


| Company: |  | Date: | $2 / 4 / 2022$ |
| :--- | :--- | :--- | :--- |
| Engineer: |  | Page: | $2 / 5$ |
| Project: |  |  |  |
| Address: |  |  |  |
| Phone: |  |  |  |
| E-mail: |  |  |  |

## Load and Geometry

Load factor source: ACI 318 Section 5.3
Load combination: $\mathrm{U}=0.9 \mathrm{D}+1.0 \mathrm{E}$
Seismic design: Yes
Anchors subjected to sustained tension: Not applicable
Ductility section for tension: 17.2.3.4.3 (c) is satisfied
Ductility section for shear: 17.2.3.5.2 not applicable
$\Omega_{0}$ factor: not set
Apply entire shear load at front row: No
Anchors only resisting wind and/or seismic loads: Yes

| Service level loads: |  |  |  |
| :--- | :--- | :--- | :--- |
|  | D | E |  |
| $\mathrm{N}_{\mathrm{a}}[\mathrm{lb}]:$ | 0 | 7700 | 7 trength level loads |
| $\mathrm{V}_{\mathrm{ax}}[\mathrm{lb]}]:$ | 0 | 0 | 0 |
| $\mathrm{~V}_{\text {ay }}[\mathrm{bb}]:$ | 0 | 0 | 0 |

<Figure 1>


<Figure 2>


## SIMPSON Anchor Designer ${ }^{\text {TM }}$ <br> Stronghtic <br> Software <br> Version 2.8.7094.0

| Company: |  | Date: | $2 / 4 / 2022$ |
| :--- | :--- | :--- | :--- |
| Engineer: |  | Page: | $4 / 5$ |
| Project: |  |  |  |
| Address: |  |  |  |
| Phone: |  |  |  |
| E-mail: |  |  |  |

3. Resulting Anchor Forces

| Anchor | Tension load, <br> $\mathrm{N}_{\text {ua }}(\mathrm{lb})$ | Shear load $x$, <br> $\mathrm{V}_{\text {uax }}(\mathrm{lb})$ | Shear load y, <br> $\mathrm{V}_{\text {uay }}(\mathrm{lb})$ | Shear load combined, <br> $\left.V_{\text {uax }}\right)^{2}+\left(\mathrm{V}_{\text {uay }}\right)^{2}(\mathrm{lb})$ |
| :--- | :--- | :--- | :--- | :--- |
| 1 | 7700.0 | 0.0 | 0.0 | 0.0 |
| Sum | 7700.0 | 0.0 | 0.0 | 0.0 |

Maximum concrete compression strain (\%): 0.00
Maximum concrete compression stress (psi): 0
Resultant tension force (lb): 7700
Resultant compression force (lb): 0
Eccentricity of resultant tension forces in x-axis, e' ${ }_{n x}$ (inch): 0.00
Eccentricity of resultant tension forces in y-axis, e' Ny (inch): 0.00

## 4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

| $N_{\text {sa }}(\mathrm{lb})$ | $\phi$ | $\phi N_{\text {sa }}$ (b) |
| :--- | :--- | :--- |
| 26795 | 0.75 | 20096 |

## 5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$N_{b}=k_{c} \lambda_{a} \sqrt{ } f_{c}^{\prime} h_{e f}{ }^{1.5}$ (Eq. 17.4.2.2a)

| $k_{c}$ | $\lambda_{a}$ | $f^{\prime} c(\mathrm{psi})$ | $h_{e f}(\mathrm{in})$ | $N_{b}(\mathrm{lb})$ |
| :--- | :--- | :--- | :--- | :--- |
| 24.0 | 1.00 | 2500 | 9.000 | 32400 |

$0.75 \phi N_{c b}=0.75 \phi\left(A_{N c} / A_{N c o}\right) \Psi_{e d, N} \Psi_{c, N} \Psi_{c p, N} N_{b}$ (Sec. 17.3.1 \& Eq. 17.4.2.1a)

| $A_{N c}\left(\mathrm{in}^{2}\right)$ | $A_{N c o}\left(\right.$ in $^{2}$ | $C_{a, \min }$ (in) | $\Psi_{e d, N}$ | $\Psi_{c, N}$ | $\Psi_{c p, N}$ | $N_{b}(\mathrm{lb})$ | $\phi$ | $0.75 \phi N_{c b}$ (lb) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 529.88 | 729.00 | 9.00 | 0.900 | 1.00 | 1.000 | 32400 | 0.75 | 11922 |

## 6. Pullout Strength of Anchor in Tension (Sec. 17.4.3)

$0.75 \phi N_{p n}=0.75 \phi \Psi_{c, P} N_{p}=0.75 \phi \Psi_{c, P 8} A_{\text {brg }} f_{c}^{\prime}($ Sec. 17.3.1, Eq. 17.4.3.1 \& 17.4.3.4)

| $\Psi_{c, P}$ | $A_{\text {brg }}\left(\right.$ in $\left.^{2}\right)$ | $f_{c}^{\prime}(\mathrm{psi})$ | $\phi$ | $0.75 \phi N_{\text {pn }}(\mathrm{lb})$ |
| :--- | :--- | :--- | :--- | :--- |
| 1.0 | 4.07 | 2500 | 0.70 | 42683 |


| Company: |  | Date: | $2 / 4 / 2022$ |
| :--- | :--- | :--- | :--- |
| Engineer: |  | Page: | $5 / 5$ |
| Project: |  |  |  |
| Address: |  |  |  |
| Phone: |  |  |  |
| E-mail: |  |  |  |

## 11. Results

11. Interaction of Tensile and Shear Forces (Sec. D.7)?

| Tension | Factored Load, Nua (lb) | Design Strength, $ø N_{n}(\mathrm{lb})$ | Ratio | Status |
| :--- | :--- | :--- | :--- | :--- |
| Steel | 7700 | 20096 | 0.38 | Pass |
| Concrete breakout | 7700 | 11922 | $\mathbf{0 . 6 5}$ | Pass (Governs) |
| Pullout | 7700 | 42683 | 0.18 | Pass |

PAB7 (7/8"Ø) with hef $=9.000$ inch meets the selected design criteria.

## 12. Warnings

- Minimum spacing and edge distance requirement of 6da per ACI 318 Sections 17.7.1 and 17.7.2 for torqued cast-in-place anchor is waived per designer option.
- Per designer input, ductility requirements for tension have been determined to be satisfied - designer to verify.
- Per designer input, the shear component of the strength-level earthquake force applied to anchors does not exceed 20 percent of the total factored anchor shear force associated with the same load combination. Therefore the ductility requirements of ACI 318 17.2.3.5.2 for shear need not be satisfied - designer to verify.
- Designer must exercise own judgement to determine if this design is suitable.


## Cantilevered Retaining Wall

DESCRIPTION: Garage/ADU Step (12/S3.2)
Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=6.00 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 0.00 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 6.00 in |
| Water height over heel | $=0.0 \mathrm{ft}$ |  |


\section*{Surcharge Loads <br> Surcharge Over Heel $\quad$| 40.0 psf |
| :---: |
| Used To Resist Sliding \& Overturning |
| Surcharge Over Toe |
| Used for Sliding \& Overturning |$\quad .0 .0$}

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 210.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 560.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Axial Load Eccentricity = 0.0 in


## Lateral Load Applied to Stem

| Lateral Load | $=$ | $0.0 \mathrm{\#} / \mathrm{ft}$ |
| :--- | :--- | :---: |
| $\ldots$. Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind (W) |
|  | (Service Level) |  |
|  |  |  |
| Wind on Exposed Stem  <br> (Strength Level) 0.0 psf |  |  |



| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| Base Above/Below Soil | $=$ | 0.0 ft |
| $\begin{array}{lll}\text { at Back of Wall } & & 0.300\end{array}$ Poisson's Ratio |  |  |

## Cantilevered Retaining Wall

DESCRIPTION: Garage/ADU Step (12/S3.2)


## Cantilevered Retaining Wall

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

Summary of Overturning \& Resisting Forces \& Moments


Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.070 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall
Project File: Foundations.ec6
LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021 DESCRIPTION: Garage/ADU Step (12/S3.2)


Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



## Cantilevered Retaining Wall

## DESCRIPTION: SE Den/Guest Rm (9/S3.2)

## Code Reference.

Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=4.00 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 0.50 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 6.00 in |
| Water height over heel | $=$ | 0.0 ft |


\section*{Surcharge Loads <br> Surcharge Over Heel $\quad$| 40.0 psf |
| :---: |
| Used To Resist Sliding \& Overturning |
| Surcharge Over Toe |
| Used for Sliding \& Overturning |$\quad .0 .0$}

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 120.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 40.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Axial Load Eccentricity $=0.0$ in

| Allow Soil Bearing $\quad=4,0$ Equivalent Fluid Pressure Method |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Active Heel Pressure | = | 40.0 psf/ft |
|  | = |  |
| Passive Pressure | = | 525.0 psf/ft |
| Soil Density, Heel | = | 130.00 pcf |
| Soil Density, Toe | = | 130.00 pcf |
| Footing\||Soil Friction | = | 0.675 |
| Soil height to ignore for passive pressure |  | 12.00 in |

## Lateral Load Applied to Stem

| Lateral Load | $=$ | $0.0 \# / \mathrm{ft}$ |
| :--- | :--- | :---: |
| $\ldots$. Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind (W) |
|  |  | (Service Level) |
|  |  |  |
| Wind on Exposed Stem  <br> (Strength Level)  | 0.0 pst |  |



| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| Base Above/Below Soil | $=$ | 0.0 ft |
| $\begin{array}{lll}\text { at Back of Wall } & & 0.300\end{array}$. |  |  |

## Cantilevered Retaining Wall

## DESCRIPTION: SE Den/Guest Rm (9/S3.2)



## Cantilevered Retaining Wall

## DESCRIPTION: SE Den/Guest Rm (9/S3.2)

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

DESCRIPTION: SE Den/Guest Rm (9/S3.2)
Summary of Overturning \& Resisting Forces \& Moments


Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |  |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.131 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall




Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall

## Cantilevered Retaining Wall

Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=20.67 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 0.00 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 0.00 in |
| Water height over heel | $=$ | 0.0 ft |

## Surcharge Loads <br> Surcharge Over Heel $\quad \overline{=} \quad 0.0 \mathrm{psf}$ Used To Resist Sliding \& Overturning Surcharge Over Toe $=0.0$ Used for Sliding \& Overturning

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 0.0 lbs |
| :--- | :--- | :--- |
| Axial Live Load | $=$ | 0.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Axial Load Eccentricity $=0.0$ in

| Allow Soil Bearing $=4,0$ Equivalent Fluid Pressure Method |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Active Heel Pressure | = | 10.0 psf/ft |
|  |  |  |
| Passive Pressure | = | 525.0 pst/ft |
| Soil Density, Heel | = | 10.00 pcf |
| Soil Density, Toe | = | 130.00 pcf |
| Footing\||Soil Friction | = | 0.525 |
| Soil height to ignore for passive pressure | = | 0.00 in |

## Lateral Load Applied to Stem

| Lateral Load | $=$ | $0.0 \# / \mathrm{ft}$ |
| :--- | :--- | :---: |
| $\ldots$ Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind $(\mathrm{W})$ |
|  |  | $($ Service Level) |



| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| Base Above/Below Soil | $=$ | 0.0 ft |
| $\begin{array}{lll}\text { at Back of Wall } & & 0.300\end{array}$. |  |  |

## Cantilevered Retaining Wall

DESCRIPTION: Garage Wall (12/S3.3)


## Cantilevered Retaining Wall

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

DESCRIPTION: Garage Wall (12/S3.3)

## Summary of Overturning \& Resisting Forces \& Moments



|  | Force lbs | $\begin{gathered} \text { SISTING..... } \\ \text { Dt } \end{gathered}$ | Moment ft-\# |
| :---: | :---: | :---: | :---: |
| Soil Over HL (ab. water tbl) | 206.7 | 7.50 | 1,550.0 |
| Soil Over HL (bel. water tbl) |  | 7.50 | 1,550.0 |
| Watre Table |  |  |  |
| Sloped Soil Over Heel |  |  |  |
| Surcharge Over Heel |  |  |  |
| Adjacent Footing Load |  |  |  |
| Axial Dead Load on Stem $=$ |  |  |  |
| * Axial Live Load on Stem = |  |  |  |
| Soil Over Toe |  |  |  |
| Surcharge Over Toe |  |  |  |
| Stem Weight(s) | 3,100.1 | 6.50 | 20,150.3 |
| Earth @ Stem Transitions= |  |  |  |
| Footing Weight | 1,500.0 | 4.00 | 6,000.0 |
| Key Weight | 150.0 | 0.50 | 75.0 |
| Vert. Component |  |  |  |
| Total $=$ <br> * Axial live load NOT included resistance, but is included for | 4,956.7 total displa oil pressur | bs R.M.= d, or used for calculation. | $\begin{gathered} 27,775.4 \\ \text { overturning } \end{gathered}$ |

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.115 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall

Project File: Foundations.ec6
LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021

DESCRIPTION: Garage Wall (12/S3.3)


Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



## Cantilevered Retaining Wall

## Code Reference.

Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :---: |
| Retained Height | $=19.00 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 0.00 ft |
| Slope Behind Wall | $=0.00$ |  |
| Height of Soil over Toe | $=$ | 0.00 in |
| Water height over heel | $=$ | 0.0 ft |

## Surcharge Loads <br> Surcharge Over Heel $\quad=\quad 0.0 \mathrm{psf}$ Used To Resist Sliding \& Overturning Surcharge Over Toe $\quad=\quad 0.0$ Used for Sliding \& Overturning

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 120.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 300.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Axial Load Eccentricity $=0.0$ in

| Allow Soil Bearing $\quad=4,0$ Equivalent Fluid Pressure Method |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Active Heel Pressure | = | 10.0 psf/ft |
|  | = |  |
| Passive Pressure | = | 525.0 psf/ft |
| Soil Density, Heel | = | 5.00 pcf |
| Soil Density, Toe | = | 130.00 pcf |
| Footing\||Soil Friction | = | 0.525 |
| Soil height to ignore for passive pressure |  | 0.00 in |

## Lateral Load Applied to Stem

| Lateral Load | $=$ | $0.0 \# / \mathrm{ft}$ |
| :--- | :--- | :---: |
| $\ldots$ Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind $(\mathrm{W})$ |
|  |  |  |
|  | (Service Level) |  |
| Wind on Exposed Stem |  | 0.0 psf |
| (Strength Level)   |  |  |



## Cantilevered Retaining Wall

DESCRIPTION: Stair Wall (10/S3.1)


## Cantilevered Retaining Wall

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

DESCRIPTION: Stair Wall (10/S3.1)

## Summary of Overturning \& Resisting Forces \& Moments



Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.138 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



DESCRIPTION: SE \& NW Den/Guest Rm (11/S3.2)
Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16


| Design Summary |  |
| :---: | :---: |
| Total Bearing Load ...resultant ecc. | $\begin{array}{ll} = & 1,757.50 \mathrm{lbs} \\ = & -0.9165 \mathrm{in} \end{array}$ |
| Soil Pressure @ Toe | 699.39 psf OK |
| Soil Pressure @ Heel | 1,140.93 psf OK |
| Allowable Soil Pressure Les | $=\text { Than Allowable }{ }^{\mathrm{psf}}$ |
| ACI Factored @ Toe ACI Factored @ Heel | $\begin{array}{r} 845.63 \mathrm{psf} \\ 1,379.50 \mathrm{psf} \end{array}$ |
| Footing Shear @ Toe | 0.2481 psi OK |
| Footing Shear @ Heel Allowable | $\begin{aligned} & -0.1707 \mathrm{psi} \text { OK } \\ & 75.0 \mathrm{psi} \end{aligned}$ |
| Reaction at Top | 1,446.16 lbs |
| Reaction at Bottom | 536.86 lbs |
| Sliding Calcs <br> Lateral Sliding Force | $=536.86 \mathrm{lbs}$ |

Vertical component of active lateral soil pressure IS NOT considered in the calculation of soil bearing

| Soil Data |  |  |
| :---: | :---: | :---: |
| Allow Soil Bearing |  | 4,000.0 psf |
| Equivalent Fluid Pressure Method |  |  |
| At-Rest Heel Pressure | = | $55.0 \mathrm{psf} / \mathrm{ft}$ |
|  | = | $0.0 \mathrm{pst} / \mathrm{ft}$ |
| Passive Pressure | = | 525.0 pst/ft |
| Soil Density | = | 130.0 pcf |
| Footing\||Soil Frictior | = | 0.5250 psf |
| Soil height to ignore for passive pressure | = | in |


| Uniform Lateral Load Applied to Stem |  |  |
| :--- | :--- | :--- |
| Lateral Load | $=$ | $\# / \mathrm{ft}$ |
| $\ldots$ Height to Top | $=$ | ft |
| $\ldots$ Height to Bottom | $=$ | ft |
| Load Type | $=$ | Wind (W) |
| (Service Level) |  |  |
| Wind on Exposed Stem | $=$0.00 psf <br> (Strength Level) |  |
| Wind acts left-to-right toward retention side. |  |  |

$\mathrm{K}_{\mathrm{h}}$ Soil Density Multiplier $=0.2 \mathrm{~g} \quad$ Added seismic per unit area $=0.0 \mathrm{psf}$

| Concrete Stem Construction |
| :--- |
| Thickness $=\quad 8.00 \mathrm{in}$ |
| Wall Weight $=\quad 100.0 \mathrm{psf}$ |
| Stem is FREE to rotate at top of footing |


|  | @ Top Support | Mmax Between Top \& Base | @ Base of Wall |
| :---: | :---: | :---: | :---: |
|  | Stem OK | Stem OK | Stem OK |
| Design Height Above Ftg | 2.667 ft | 0.2463 ft | 0.00 ft |
| Rebar Size | \# 4 | \# 4 | \# 4 |
| Rebar Spacing | 12.00 in | 12.00 in | 12.00 in |
| Rebar Placed at | Edge | Edge | Edge |
| Rebar Depth 'd' | 5.50 in | 6.0 in | 5.50 in |
| Design Data $\mathrm{fb} / \mathrm{FB}+\mathrm{fa} / \mathrm{Fa}$ |  |  |  |
| Moment....Actual | $=1,655.70 \mathrm{ft}-\mathrm{\#}$ | 18.387 ft -\# | $0.0 \mathrm{ft-} \mathrm{\#}$ |
| Moment.....Allowable | $=4,737.60 \mathrm{ft}-\mathrm{\#}$ | 5,187.60 ft-\# | 4,737.60 ft-\# |
| Shear Force @ this height | $=1,292.28 \mathrm{lbs}$ |  | 154.978 lbs |
| Shear.....Actual | $=19.580 \mathrm{psi}$ |  | 2.348 psi |
| Shear.....Allowable | 75.0 psi |  | 75.0 psi |


| Load Factors |  |
| :--- | :--- |
| $\quad$ Building Code |  |
| Dead Load | 0.000 |
| Live Load | 0.000 |
| Earth, H | 0.000 |
| Wind, W | 0.000 |
| Seismic, E | 0.000 |

## Restrained Retaining Wall

DESCRIPTION: SE \& NW Den/Guest Rm (11/S3.2)

## Footing Strengths \& Dimensions

| Toe Width | $=$ | 0.750 ft |
| :--- | :--- | :---: |
| Heel Width | $=$ | 1.160 |
| Total Footing Widtr | $=$ | 1.910 |
| Footing Thickness | $=$ | 12.0 in |
| Key Width | $=$ | in |
| Key Depth | $=$ | in |
| Key Distance from Toe | $=$ | ft |
| f'c = 2,500.0 psi Fy | $=$ | 60000 psi |
| Footing Concrete Density | $=$ | 150 pcf |
| Min. As \% | $=$ | 0.0018 |
| Cover @ Top = 2 in | @ Btm.= | 3 in |

Footing Design Results

|  |  |  |  |
| :--- | :--- | ---: | ---: |
|  |  | Toe | $\underline{\text { Heel }}$ |
| Factored Pressure | $=$ | 845.63 | $1,379.50 \mathrm{psf}$ |
| $\mathrm{Mu}^{\prime}:$ Upward | $=$ | 257.488 | $\mathrm{ft}-\#$ |
| $\mathrm{Mu}^{\prime}:$ Downward | $=$ | 68.625 | $\mathrm{ft}-\#$ |
| Mu: Design | $=$ | 189 | $-4 \mathrm{ft}-\#$ |
| Actual 1-Way Shear | $=$ | 0.2481 | psi |
| Allow 1-Way Shear | $=$ | 75.0 | 75.0 psi |


| Other Acceptable Sizes \& Spacings: |  |
| :---: | :---: |
| Toe: \# 7 @ 18.00 in -or- | -or- phiMn $=$ phi * 5 * lambda * sqrt(fc) * Sm |
| Heel:None Spec'd -or- | -or- phiMn $=$ phi * 5 * lambda * sqrt(fc) * Sm |
| Key: \# 0 @ 0.00 in -or- | -or- No key defined |
| Min footing T\&S reinf Area | 0.50 in2 |
| Min footing T\&S reinf Area per foot | oot 0.26 in2 ft |
| If one layer of horizontal bars: If | If two layers of horizontal bars: |
| \#4@ 9.26 in | \#4@18.52 in |
| \#5@ 14.35 in | \#5@ 28.70 in |
| \#6@ 20.37 in | \#6@ 40.74 in |

## Summary of Forces on Footing : Slab is NOT resisting sliding, stem is PINNED at footing



[^0] the calculation of Sliding Resistance.

Project Title:
Engineer:
Project ID:
Project Descr:

Restrained Retaining Wall


Project Title:
Engineer:
Project ID:
Project Descr:

Restrained Retaining Wall


## Cantilevered Retaining Wall

DESCRIPTION: SW Den/Guest Rm (10/S3.2)
Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :---: |
| Retained Height | $=$ | 7.17 ft |
| Wall height above soil | $=$ | 2.92 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 48.00 in |
| Water height over heel | $=$ | 0.0 ft |

## Surcharge Loads <br> Surcharge Over Heel $\quad=\quad 40.0 \mathrm{psf}$ Used To Resist Sliding \& Overturning Surcharge Over Toe $=0.0$ Used for Sliding \& Overturning

## Axial Load Applied to Stem

| Axial Dead Load | $=$ | 120.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 40.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Axial Load Eccentricity $=0.0$ in


## Lateral Load Applied to Stem

| Lateral Load | $=$ | $0.0 \mathrm{\#} / \mathrm{ft}$ |
| :--- | :--- | :---: |
| $\ldots$. Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind (W) |
|  | (Service Level) |  |
|  |  |  |
| Wind on Exposed Stem  <br> (Strength Level) 0.0 psf |  |  |



| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| Base Above/Below Soil | $=$ | 0.0 ft |
| at Back of Wall | $=$ | 0.300 |

## Cantilevered Retaining Wall

DESCRIPTION: SW Den/Guest Rm (10/S3.2)


## Cantilevered Retaining Wall

DESCRIPTION: SW Den/Guest Rm (10/S3.2)

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

DESCRIPTION: SW Den/Guest Rm (10/S3.2)

## Summary of Overturning \& Resisting Forces \& Moments



Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.300 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall

8" w/ \#4@10"

\#4@12in
@ Toe


Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall <br> Project File: Foundations.ec6

LIC\# : KW-06015393, Build:20.22.1.19 BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021

DESCRIPTION: SW Den/Guest Rm (10/S3.2)


## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU/Laundry W/ 9H (12/S3.1)
Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=6.50 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 3.59 ft |
| Slope Behind Wall | $=0.00$ |  |
| Height of Soil over Toe | $=0.00 \mathrm{in}$ |  |
| Water height over heel | $=0.0 \mathrm{ft}$ |  |

## Surcharge Loads

Surcharge Over Heel $\quad \overline{\overline{2}} \quad 40.0 \mathrm{psf}$
Used To Resist Sliding
Surcharge Over Toe
Overturning
Used for Sliding \& Overturning

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 290.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 435.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Earth Pressure Seismic Load
Method: Uniform
Multiplier Used
(Multiplier used on soil density)

| Allow Soil Bearing $=4,0$ Equivalent Fluid Pressure Method |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Active Heel Pressure | = | $55.0 \mathrm{psf} / \mathrm{ft}$ |
|  |  |  |
| Passive Pressure | = | 525.0 pst/ft |
| Soil Density, Heel | = | 130.00 pcf |
| Soil Density, Toe | = | 130.00 pcf |
| Footing\||Soil Friction | = | 0.675 |
| Soil height to ignore for passive pressure | = | 0.00 in |

## Lateral Load Applied to Stem

| Lateral Load | 0.0 \#/ft |
| :---: | :---: |
| ...Height to Top | 0.00 ft |
| ...Height to Bottom | 0.00 ft |
| Load Type | $\begin{aligned} = & \text { Wind (W) } \\ & \text { (Service Level) } \end{aligned}$ |
| Wind on Exposed Stem (Strength Level) | 0.0 psf |


| Uniform Seismic Force | $=$ | 67.500 |
| :--- | :--- | ---: |
| Total Seismic Force | $=$ | 506.250 |



| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| $\begin{array}{llc}\text { Base Above/Below Soil } & = & 0.0 \mathrm{ft} \\ \text { at Back of Wall } & = & 0.300\end{array}$. |  |  |

Cantilevered Retaining Wall Project File: Foundations.ec6

DESCRIPTION: SE @ ADU/Laundry W/ 9H (12/S3.1)


## Cantilevered Retaining Wall

LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021

DESCRIPTION: SE @ ADU/Laundry W/ 9H (12/S3.1)

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU/Laundry W/ 9H (12/S3.1)

## Summary of Overturning \& Resisting Forces \& Moments

|  |  | $\begin{array}{c}\text { Force } \\ \text { Ibs }\end{array}$ |  | $\begin{array}{c}\text { OVERTURNING..... } \\ \text { Distance } \\ \mathrm{ft}\end{array}$ |
| :--- | :---: | :---: | :---: | :---: | \(\left.\begin{array}{c}Moment <br>

\mathrm{ft}-\mathrm{\#}\end{array}\right]\)

| Resisting/Overturning Ratio | $=$ |
| :--- | :--- |
| Vertical Loads used for Soil Pressure $=$ | $\mathbf{1 . 8 3}$ |
| $4,031.2 \mathrm{lbs}$ |  |

If seismic is included, the OTM and sliding ratios
may be 1.1 per section 1807.2.3 of IBC.
Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.118 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU/Laundry (12/S3.1)
Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=7.17 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 3.00 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 0.00 in |
| Water height over heel | $=0.0 \mathrm{ft}$ |  |

## Surcharge Loads <br> Surcharge Over Heel $\quad=\quad 40.0 \mathrm{psf}$ Used To Resist Sliding \& Overturning Surcharge Over Toe $\quad=\quad 0.0$ Used for Sliding \& Overturning

Axial Load Applied to Stem

| Axial Dead Load | $=290.0 \mathrm{lbs}$ |  |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 435.0 lbs |
| Axial Load Eccentricity | $=0.0 \mathrm{in}$ |  |

Axial Load Eccentricity $=0.0$ in

| Allow Soil Bearing $=4,0$ Equivalent Fluid Pressure Method |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Active Heel Pressure | = | $55.0 \mathrm{psf} / \mathrm{ft}$ |
|  |  |  |
| Passive Pressure | = | 525.0 pst/ft |
| Soil Density, Heel | = | 130.00 pcf |
| Soil Density, Toe | = | 130.00 pcf |
| Footing\||Soil Friction | = | 0.675 |
| Soil height to ignore for passive pressure | = | 0.00 in |


| Lateral Load Applied to Stem |  |  |
| :--- | :--- | :---: |
| Lateral Load | $=$ | $0.0 \mathrm{\#} / \mathrm{ft}$ |
| $\ldots$ Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind (W) |
|  | (Service Level) |  |
| Wind on Exposed Stem |  | 0.0 psf |
| (Strength Level)  |  |  |




## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU/Laundry (12/S3.1)


## Cantilevered Retaining Wall

LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
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DESCRIPTION: SE @ ADU/Laundry (12/S3.1)

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021

DESCRIPTION: SE @ ADU/Laundry (12/S3.1)
Summary of Overturning \& Resisting Forces \& Moments


Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.102 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall

## Cantilevered Retaining Wall

Code Reference.
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=$ | 6.00 ft |
| Wall height above soil | $=$ | 0.50 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 6.00 in |
| Water height over heel | $=$ | 0.0 ft |

## Surcharge Loads <br> Surcharge Over Heel $\quad=\quad 0.0 \mathrm{psf}$ Used To Resist Sliding \& Overturning Surcharge Over Toe $\quad=\quad 0.0$ Used for Sliding \& Overturning

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 290.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 435.0 lbs |
| Axial Load Eccentricity | $=$ | 0.0 in |

Axial Load Eccentricity $=0.0$ in


## Lateral Load Applied to Stem

| Lateral Load | $=$ | $0.0 \# / \mathrm{ft}$ |
| :--- | :--- | :---: |
| $\ldots$ Height to Top | $=$ | 0.00 ft |
| $\ldots$ Height to Bottom | $=$ | 0.00 ft |
| Load Type | $=$ | Wind $(\mathrm{W})$ |
|  |  | $($ Service Level) |



| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| $\begin{array}{llc}\text { Base Above/Below Soil } & & 0.0 \mathrm{ft} \\ \text { at Back of Wall } & & 0.300\end{array} \quad \begin{array}{ll}\text { Poisson's Ratio } & =\end{array}$ |  |  |

## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU (4/S3.1)


| Cantilevered Retaining Wall |  |
| :--- | :--- | :--- |
| LIC\#: KW -06015393, Buidd:20.22.1.19 | Project File: Foundations.ec6 |

LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
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DESCRIPTION: SE @ ADU (4/S3.1)

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

LIC\# : KW-06015393, Build:20.22.1.19
BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021

DESCRIPTION: SE @ ADU (4/S3.1)
Summary of Overturning \& Resisting Forces \& Moments

| Item | ${ }_{\text {Force }}^{\text {lbs }}$ | $\begin{aligned} & \text { ERTURNING...... } \\ & \text { Distance } \\ & \mathrm{ft} \end{aligned} \underset{\mathrm{ft}-\mathrm{\#}}{\text { Moment }}$ |  | ..RESISTING..... |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Force lbs | Distance ft | Moment ft-\# |
| HL Act Pres (ab water tbl) | 980.0 | 2.33 | 2,286.7 | Soil Over HL (ab. water tbl) | 390.3 | $\begin{aligned} & 2.92 \\ & 2.92 \end{aligned}$ | $\begin{aligned} & 1,138.3 \\ & 1,138.3 \end{aligned}$ |
| HL Act Pres (be water tbl) |  |  |  | Soil Over HL (bel. water tbl) |  |  |  |
| Hydrostatic Force |  |  |  | Watre Table |  |  |  |
| Buoyant Force |  |  |  |  | Sloped Soil Over Heel |  |  |  |
| Surcharge over Heel |  |  |  | Surcharge Over Heel |  |  |  |
| Surcharge Over Toe |  |  |  | Adjacent Footing Load = |  |  |  |
| Adjacent Footing Load |  |  |  | Axial Dead Load on Stem = | 290.0 | 2.33 | 676.7 |
| Added Lateral Load |  |  |  | * Axial Live Load on Stem = | 435.0 | 2.33 | 1,015.0 |
| Load @ Stem Above Soil |  |  |  | Soil Over Toe | 130.0 | 1.00 | 130.0 |
|  |  |  |  | Surcharge Over Toe |  |  |  |
|  |  |  |  | Stem Weight(s) = | 650.0 | 2.33 | 1,516.7 |
| Total | 980.0 | O.T.M. |  | Earth @ Stem Transitions= |  |  | 752.2 |
|  |  |  | 2,286.7 | Footing Weight | 475.1 | 1.58 |  |
|  |  |  |  | Key Weight |  |  |  |
| Resisting/Overturning Ratio |  | $=1.84$ |  | Vert. Component |  |  |  |
| Vertical Loads used for Soil Pressure $=$ |  | 2,370.3 lbs |  | Total $=1,935.3 \mathrm{lbs}$ R.M. $=\quad 4,213.9$ <br> * Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation. |  |  |  |

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.070 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall
Project File: Foundations.ec6
LIC\# : KW-06015393, Build:20.22.1.19 BYKONEN CARTER QUINN
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Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall

Project File: Foundations.ec6
LIC\# : KW-06015393, Build:20.22.1.19 BYKONEN CARTER QUINN
(c) ENERCALC INC 1983-2021

DESCRIPTION: SE @ ADU (4/S3.1)


## Cantilevered Retaining Wall

Code Reference:
Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

| Criteria |  |  |
| :--- | :--- | :--- |
| Retained Height | $=6.00 \mathrm{ft}$ |  |
| Wall height above soil | $=$ | 0.50 ft |
| Slope Behind Wall | $=$ | 0.00 |
| Height of Soil over Toe | $=$ | 6.00 in |
| Water height over heel | $=0.0 \mathrm{ft}$ |  |

## Surcharge Loads

Surcharge Over Heel $\quad=\quad 0.0 \mathrm{psf}$
Used To Resist Sliding \& Overturning
Surcharge Over Toe $=0.0$
Used for Sliding \& Overturning

Axial Load Applied to Stem

| Axial Dead Load | $=$ | 290.0 lbs |
| :--- | :--- | ---: |
| Axial Live Load | $=$ | 435.0 lbs |
| Axial Load Eccentricity | $=0.0 \mathrm{in}$ |  |

Earth Pressure Seismic Load
Method: Uniform $=9.000$
Multiplier Used
(Multiplier used on soil density)
(Multiplier used on soil density)

| Soil Data |  |  |
| :--- | :--- | :--- |
| Allow Soil Bearing $=$ $4,000.0 \mathrm{psf}$ <br> Equivalent Fluid Pressure Method  <br> Active Heel Pressure $=$ $40.0 \mathrm{psf} / \mathrm{ft}$ |  |  |
|  | $=$ |  |
| Passive Pressure | $=$ | $525.0 \mathrm{psf} / \mathrm{ft}$ |
| Soil Density, Heel | $=$ | 130.00 pcf |
| Soil Density, Toe | $=$ | 130.00 pcf |
| Footing\||Soil Friction | $=$ | 0.675 |
| Soil height to ignore <br> for passive pressure | $=12.00 \mathrm{in}$ |  |

## Lateral Load Applied to Stem

| Lateral Load | 0.0 \#/ft |
| :---: | :---: |
| Height to Top | 0.00 ft |
| ...Height to Bottom | 0.00 ft |
| Load Type | $\begin{aligned} = & \text { Wind (W) } \\ & \text { (Service Level) } \end{aligned}$ |
| Wind on Exposed Stem (Strength Level) | 0.0 psf |


| Adjacent Footing Load |  |  |
| :--- | :--- | :---: |
| Adjacent Footing Load | $=$ | 0.0 lbs |
| Footing Width | $=$ | 0.00 ft |
| Eccentricity | $=$ | 0.00 in |
| Wall to Ftg CL Dist | $=$ | 0.00 ft |
| Footing Type |  | Spread Footing |
| Base Above/Below Soil $=$ 0.0 ft <br> at Back of Wall $=$ 0.300. |  |  |

## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU w/ 9H (4/S3.1)


## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU w/ 9H (4/S3.1)

## Concrete Stem Rebar Area Details



## Cantilevered Retaining Wall

DESCRIPTION: SE @ ADU w/ 9H (4/S3.1)
Summary of Overturning \& Resisting Forces \& Moments


Tilt

## Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.115 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,
because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

## Cantilevered Retaining Wall



Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall
Project File: Foundations.ec6
LIC\# : KW-06015393, Build:20.22.1.19
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DESCRIPTION: SE @ ADU w/ 9H (4/S3.1)


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| Title H=7' : |  | Page : 2 |
| :--- | :--- | :---: |
| Dsgnr: JAJ |  |  |
| Description.... | Date: | 25 JAN 2022 |

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## Concrete Stem Rebar Area Details

| Bottom Stem | Vertical |
| :---: | :---: |
| As (based on applied moment) : | 0.1033 |
| (4/3) * As : | 0.1378 |
| 200bd/fy : 200(12)(8.1875)/60000 | 0.3275 |
| 0.0018bh : 0.0018(12)(10) : | 0.216 |
| Required Area : | 0.21 |
| Provided Area : | 0.31 in |
| Maximum Area | 1.1092 |
| Footing Data |  |
| Toe Width | 1.00 ft |
| Heel Width | 3.50 |
| Total Footing Width | 4.50 |
| Footing Thickness | 12.00 in |
| Key Width | 0.00 in |
| Key Depth | 0.00 in |
| Key Distance from Toe | 0.00 ft |
| $\begin{array}{ll}\text { f'c }= & 2,500 \mathrm{psi} \\ \text { Footing Concrete Density }\end{array}$ Fy $=\quad 60,000 \mathrm{psi}$ |  |
|  |  |
| Min. As \% | 0.0018 |
| Cover @ Top 2.00 @ Bt | $\mathrm{m}=3.00 \mathrm{in}$ |


| Horizontal Reinforcing |  |
| :---: | :---: |
| Min Stem T\&S Reinf Area 1.800 in 2 |  |
| Min Stem T\&S Reinf Area per ft of stem Height : $0.240 \mathrm{in} 2 / \mathrm{ft}$ |  |
| Horizontal Reinforcing Options : |  |
| One layer of : | Two layers of : |
| \#4@ 10.00 in | \#4@ 20.00 in |
| \#5@ 15.50 in | \#5@31.00 in |
| \#6@ 22.00 in | \#6@ 44.00 in |
| sign Results |  |
| Toe | Heel |
| 2,074 | 439 psf |
| $=11,717$ | 2,710 ft-\# |
| 1,548 | 4,523 ft-\# |
| 847 | 1,812 ft-\# |
| ear $=4.97$ | 8.15 psi |
| $=75.00$ | 75.00 psi |
| = \# 5 @ 11.48 in |  |
| = \# 5 @ 11.48 in |  |
| $=$ None Spec'd |  |
| $=$ | $0.00 \mathrm{ft-lbs}$ |
| rsion, phi Tu | 0.00 ft -lbs |

If torsion exceeds allowable, provide supplemental design for footing torsion.

## Other Acceptable Sizes \& Spacings

Toe: \#4@ 9.25 in, \#5@ 14.35 in , \#6@ 20.37 in , \#7@ 27.77 in , \#8@ 36.57 in , \#9@ 46 Heel: \#4@ 9.25 in, \#5@ 14.35 in, \#6@ 20.37 in, \#7@ 27.77 in, \#8@ 36.57 in, \#9@ 46
Key: No key defined

| Min footing T\&S reinf Area | $1.17 \quad$ in2 |
| :--- | :---: |
| Min footing T\&S reinf Area per foot | $0.26 \quad$ in2 ft |
| If one layer of horizontal bars: | If two layers of horizontal bars: |
| \#4@ 9.26 in | \#4@ 18.52 in |
| \#5@ 14.35 in | \#5@ 28.70 in |
| \#6@ 20.37 in | \#6@ 40.74 in |

Title $\quad \mathbf{H = 7}$
Dsgnr: JAJ
Description....
Page: 3

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| :--- | :--- | :--- |

Summary of Overturning \& Resisting Forces \& Moments


Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.069 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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## Concrete Stem Rebar Area Details



Title H=7' seismic
Page: 3
Dsgnr: JAJ
Date: 25 JAN 2022
Description....

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| :--- | :--- | :--- |

Summary of Overturning \& Resisting Forces \& Moments


## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.091 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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| Dsgnr: JAJ | Date: | 25 JAN 2022 |
| Description.... |  |  |

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## Concrete Stem Rebar Area Details



Title $\quad \mathbf{H}=\mathbf{6}^{\prime}$ :
Page: 3
Dsgnr: JAJ
Date: 25 JAN 2022

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| Summary of Overturning \& Resisting Forces \& Moments |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Item |  |  |  |  | Force lbs | $\begin{gathered} \text { SISTING..... } \\ \text { Distance } \end{gathered}$ | Moment $\mathrm{ft}-\mathrm{\#}$ |
| HL Act Pres (ab water tbl) | 980.0 | 2.33 | 2,286.7 |  | 1,820.0 | 2.58 | 4,701.7 |
| HL Act Pres (be water tbl) Hydrostatic Force |  |  |  | Soil Over HL (bel. water tbl) |  | 2.58 | 4,701.7 |
|  |  |  |  |  | Watre Table |  |  |  |
| Buoyant Force |  | = |  |  | Sloped Soil Over Heel |  |  |  |
| Surcharge over Heel | = |  |  | Surcharge Over Heel |  |  |  |
| Surcharge Over Toe | $=$ |  |  | Adjacent Footing Load = |  |  |  |
| Adjacent Footing Load | = |  |  | Axial Dead Load on Stem = |  |  |  |
| Added Lateral Load | $=$ |  |  | *Axial Live Load on Stem = |  |  |  |
| Load @ Stem Above Soil |  |  |  | Soil Over Toe |  | 0.38 |  |
|  | $=$ |  |  | Surcharge Over Toe |  |  |  |
|  |  |  |  | Stem Weight(s) = | 650.0 | 1.08 | 704.2 |
| Total |  | O.T.M. |  | Earth @ Stem Transitions= |  |  |  |
|  | 980.0 |  | 2,286.7 | Footing Weight | 562.5 | 1.88 | 1,054.7 |
|  |  |  |  | Key Weight |  |  |  |
| Resisting/Overturning Ratio |  | $=$$3,032.5$2.83lbs |  | Vert. Component |  |  |  |
| Vertical Loads used for | Soil Pressure |  |  | Total $=$ | 3,032.5 | (b).M.= | 6,460.5 |

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.070 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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Title H=6' seismic Page: 2
Dsgnr: JAJ
Date: 25 JAN 2022

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## Concrete Stem Rebar Area Details



Title $\mathrm{H}=6$ ' seismic
Page: 3
Dsgnr: JAJ
Date: 25 JAN 2022

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Summary of Overturning \& Resisting Forces \& Moments


If seismic is included, the OTM and sliding ratios
may be 1.1 per section 1807.2.3 of IBC.
Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.095 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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| Title H=5' : |  | Page : 2 |
| :--- | :--- | :---: |
| Dsgnr: JAJ |  |  |
| Description.... | Date: 25 JAN 2022 |  |

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## Concrete Stem Rebar Area Details



Title $\quad \mathbf{H}=5^{\prime}$ :
Page: 3
Dsgnr: JAJ
Date: 25 JAN 2022

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| :--- | :--- | :--- |
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Summary of Overturning \& Resisting Forces \& Moments


Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.077 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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Title $H=5$ ' seismic Page: 2
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## Concrete Stem Rebar Area Details

| Bottom Stem | Vertical |
| :---: | :---: |
| As (based on applied moment) : | 0.0745 |
| (4/3) * As : | 0.0994 |
| 200bd/fy : 200(12)(6.25)/60000 : | 0.25 in2 |
| 0.0018bh : 0.0018(12)(8) : | 0.1728 |
| Required Area | 0.1728 |
| Provided Area : | $0.2 \mathrm{in} 2 / \mathrm{t}$ |
| Maximum Area : | 0.8467 |
| Footing Data |  |
| Toe Width | 0.42 ft |
| Heel Width | 2.50 |
| Total Footing Width | 2.92 |
| Footing Thickness | 10.00 in |
| Key Width | 0.00 in |
| Key Depth | 0.00 in |
| Key Distance from Toe | 0.00 ft |
| $\mathrm{f}^{\prime} \mathrm{C}=\quad 2,500 \mathrm{psi} \quad \mathrm{Fy}=$ <br> Footing Concrete Density = | 60,000 psi |
|  | 150.00 pcf |
| Min. As \% | 0.0018 |
| Cover @ Top 2.00 @ | $\mathrm{m}=3.00 \mathrm{in}$ |


| Horizontal Reinforcing |  |
| :---: | :---: |
| Min Stem T\&S Reinf Area 1.056 in2 |  |
| Min Stem T\&S Reinf Area per ft of stem Height : 0.192 in2/ft |  |
| Horizontal Reinforcing Options : |  |
| One layer of : | Two layers of : |
| \#4@ 12.50 in | \#4@ 25.00 in |
| \#5@ 19.38 in | \#5@ 38.75 in |
| \#6@ 27.50 in | \#6@ 55.00 in |
| sign Results |  |
| Toe | Heel |
| 3,005 | 0 psf |
| 2,900 | 174 ft-\# |
| 237 | 1,563 ft-\# |
| 222 | 1,389 ft-\# |
| ear $=0.41$ | 12.36 psi |
| 75.00 | 75.00 psi |
| $\begin{aligned} & =\# 4 @ 11.11 \text { in } \\ & =\# 4 @ 11.11 \text { in } \\ & =\text { None Spec'd } \end{aligned}$ |  |
|  |  |
|  |  |
| Tu | $0.00 \mathrm{ft-lbs}$ |
| rsion, phi Tu | 0.00 ft -lbs |

If torsion exceeds allowable, provide supplemental design for footing torsion.

## Other Acceptable Sizes \& Spacings

Toe: \#4@ 11.11 in, \#5@ 17.22 in, \#6@ 24.44 in, \#7@ 33.33 in, \#8@ 43.88 in , \#9@ 5 Heel: \#4@ 11.11 in, \#5@ 17.22 in, \#6@ 24.44 in, \#7@ 33.33 in, \#8@ 43.88 in, \#9@ 5 Key: No key defined

| Min footing T\&S reinf Area | $0.63 \quad$ in2 |
| :--- | :--- |
| Min footing T\&S reinf Area per foot | 0.22 in2 ft |
| If one layer of horizontal bars: | If two layers of horizontal bars: |
| \#4@ 11.11 in | \#4@ 22.22 in |
| \#5@ 17.22 in | \#5@ 34.44 in |
| \#6@ 24.44 in | \#6@ 48.89 in |

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| :--- | :--- | :--- |

Summary of Overturning \& Resisting Forces \& Moments


## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.112 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe. because the wall would then tend to rotate into the retained soil.

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## Concrete Stem Rebar Area Details



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* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.062 in |  |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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| Earth Pressur | Lo |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Method : Uniform |  | Uniform Seismic Force | = | 43.500 |
| Multiplier Used | 9.000 | Total Seismic Force |  | 210.250 |

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## Concrete Stem Rebar Area Details



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| :--- | :--- | :--- |

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## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.089 in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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## Concrete Stem Rebar Area Details



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Summary of Overturning \& Resisting Forces \& Moments


* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.089 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

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## Concrete Stem Rebar Area Details



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Summary of Overturning \& Resisting Forces \& Moments


If seismic is included, the OTM and sliding ratios
may be 1.1 per section 1807.2.3 of IBC.
Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS considered in the calculation of Overturning Resistance.

## Tilt

Horizontal Deflection at Top of Wall due to settlement of soil
(Deflection due to wall bending not considered)

| Soil Spring Reaction Modulus | 250.0 | pci |
| :--- | :--- | :--- |
| Horizontal Defl @ Top of Wall (approximate only) | 0.078 | in |

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.


[^0]:    Vertical component of active lateral soil pressure IS NOT considered in

